


REMARKS

The drawings have been amended as required, by removing descriptive legends. Removed material has been inserted into the specification where appropriate, without adding new matter.

Respectfully submitted,

GREER, BURNS & CRAIN, LTD.

By 

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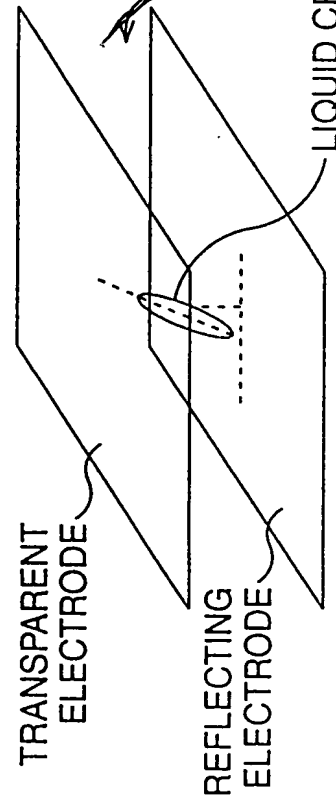
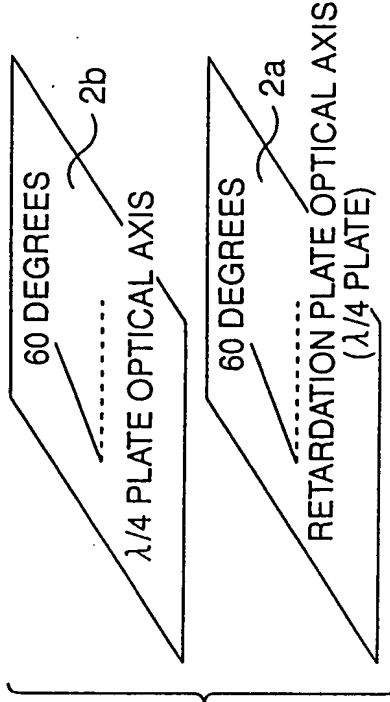
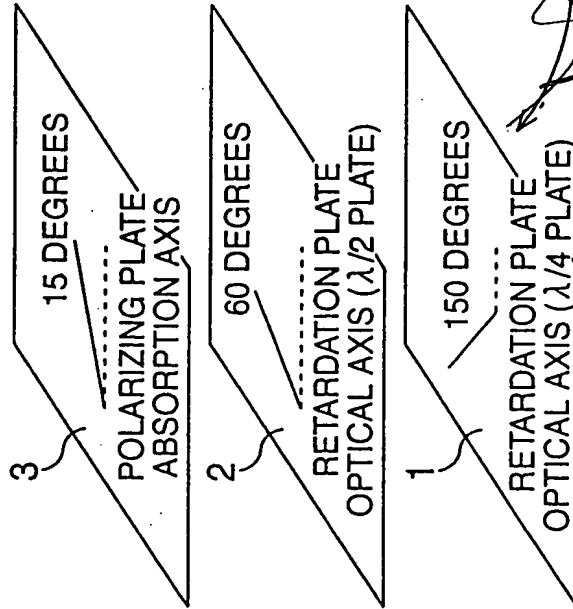
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FIG. 1

THE RETARDATION OF 2 IS OBTAINED
 BY ADDING $\lambda/4$ TO THE RETARDATION OF 2a
 THE RETARDATION OF 2 IS $\lambda/2$ WHERE
 THE RETARDATION OF 2a IS $\lambda/4$

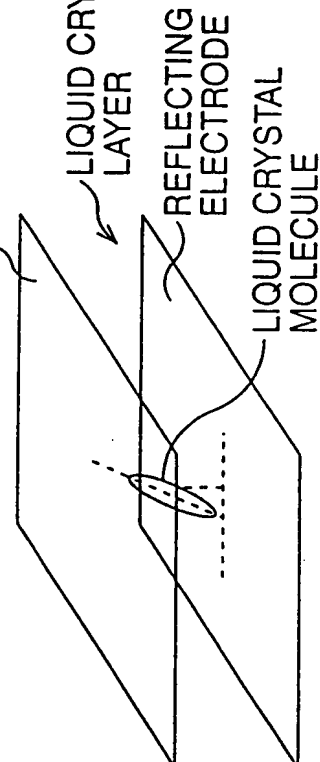
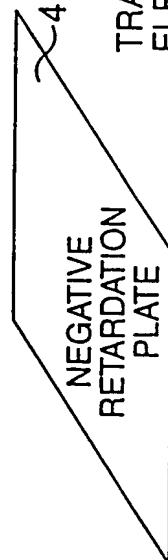
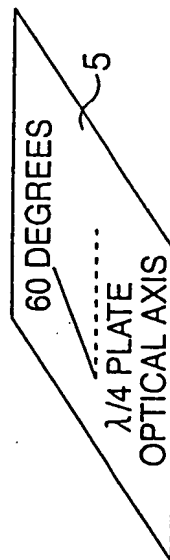
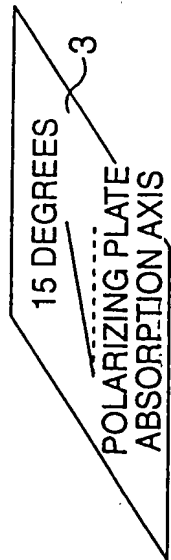


IN-PLANE RETARDATIONS CANCEL
 OUT AND ONLY NEGATIVE
 RETARDATIONS REMAIN

LIQUID CRYSTAL LAYER
 VERTICALLY ALIGNED LIQUID CRYSTAL MOLECULE
 PUTS IN A 0-DEGREE AZIMUTH WHERE VOLTAGE
 IS APPLIED

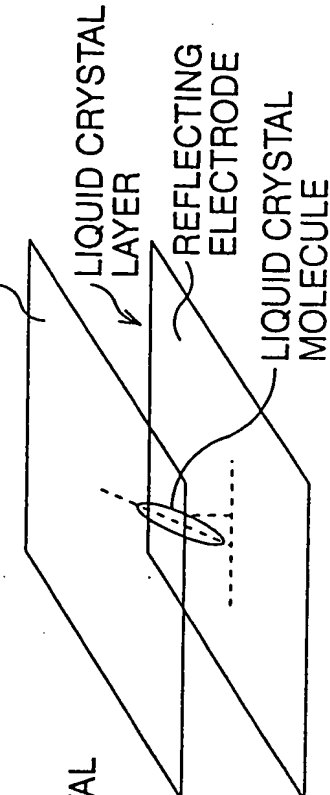
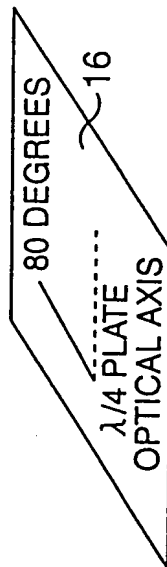
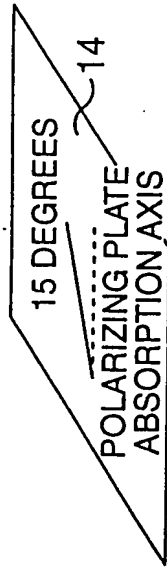
LIQUID CRYSTAL MOLECULE

FIG. 2A



VERTICALLY ALIGNED LIQUID CRYSTAL MOLECULE TILTS IN A 0-DEGREE AZIMUTH WHERE VOLTAGE IS APPLIED

FIG. 2B



VERTICALLY ALIGNED LIQUID CRYSTAL MOLECULE TILTS IN A 0-DEGREE AZIMUTH WHERE VOLTAGE IS APPLIED

FIG. 3

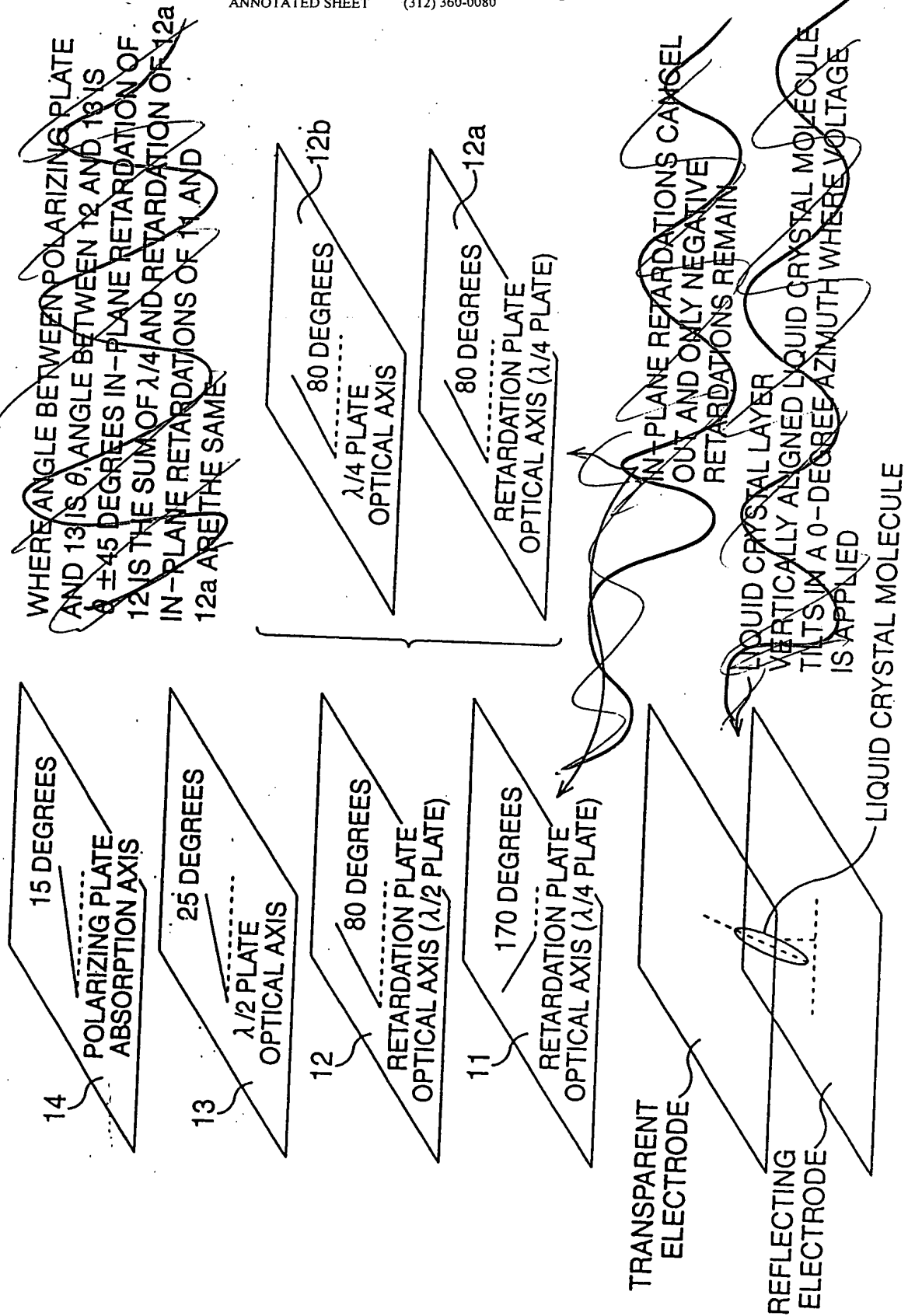
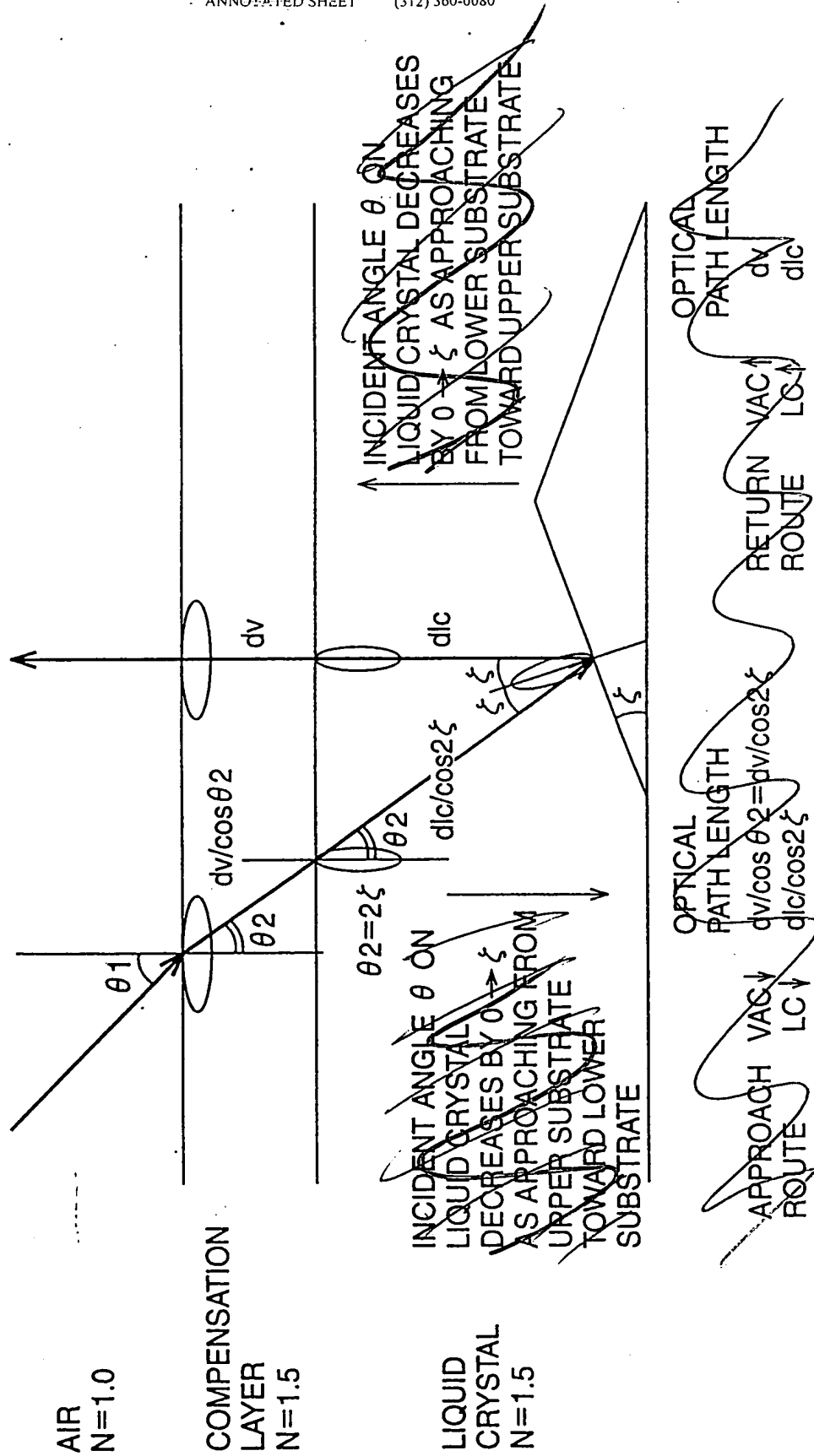
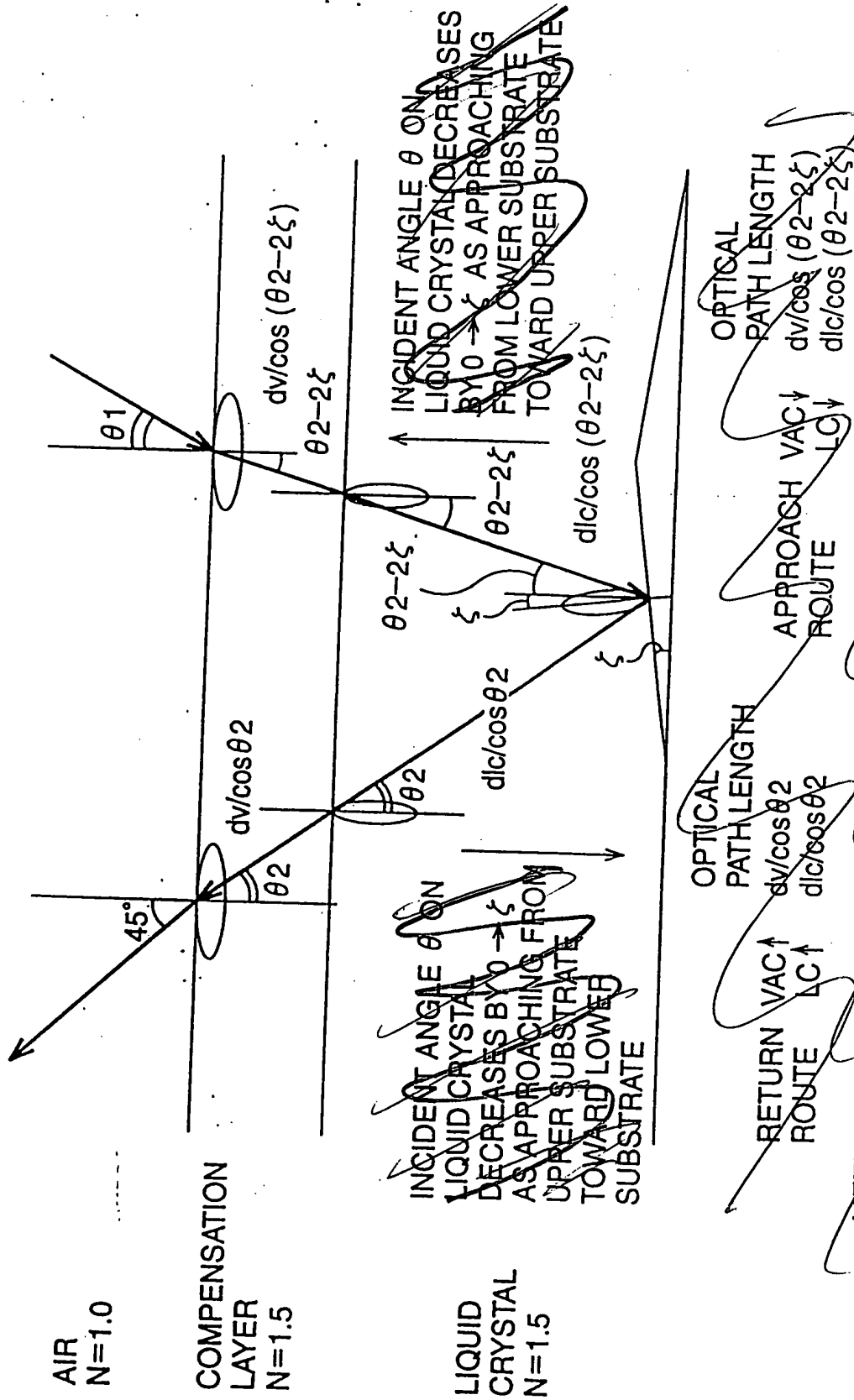


FIG. 12



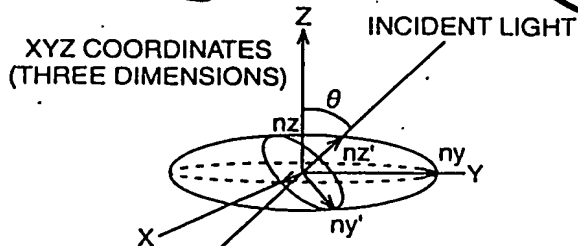
METHOD FOR ESTIMATING RETARDATION OF LIQUID CRYSTAL LAYER WHERE NO VOLTAGE IS APPLIED AND RETARDATION OF RETARDATION PLATE (OBSERVATION ANGLE OF 0°)

FIG. 13



METHOD FOR ESTIMATING RETARDATION OF LIQUID CRYSTAL LAYER, WHERE NO VOLTAGE IS APPLIED AND RETARDATION OF RETARDATION PLATE (OBSERVATION ANGLE OF 45°)

FIG. 14A



ASSUME THAT RETARDATION PLATE IS INDEX ELLIPSOID HAVING NEGATIVE REFRACTIVE INDEX ANISOTROPY IN SUBSTRATE VERTICAL DIRECTION.

YZ COORDINATES (TWO DIMENSIONS)

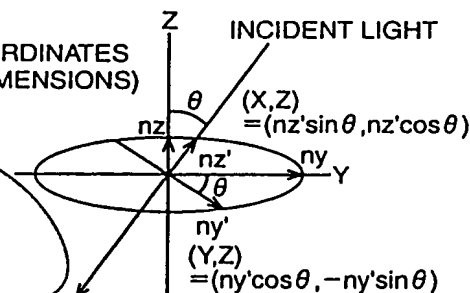
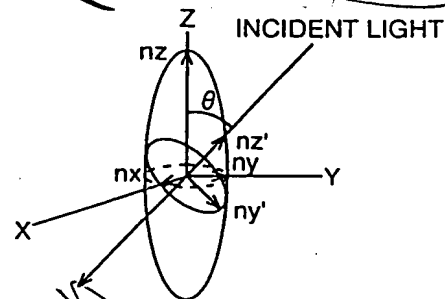


FIG. 14B

FIG. 14

FIG. 14C



ASSUME THAT LIQUID CRYSTAL IS INDEX ELLIPSOID HAVING POSITIVE REFRACTIVE INDEX ANISOTROPY IN SUBSTRATE VERTICAL DIRECTION.

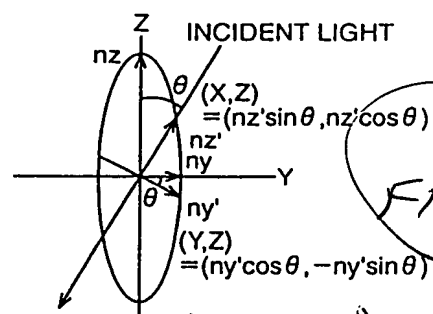


FIG. 14D

THE APPARENT REFRACTIVE INDEXES nx' , ny' , nz' WHEN LIGHT IS INCIDENT, AT AN INCIDENT ANGLE OF θ , ON XY PLANE CORRESPOND TO THE CUT SURFACE OF AN ELLIPSOID ROTATED $-\theta$ FROM THE X-AXIS, AND $nx = nx'$, ny' , nz' CAN BE FOUND BY THE FOLLOWING EQUATIONS

$$\frac{y^2}{Ny^2} + \frac{z^2}{Nz^2} = 1$$

$$\frac{Ny'^2 \cos^2 \theta}{Ny^2} + \frac{Ny'^2 \sin^2 \theta}{Nz^2} = 1$$

$$Ny'^2 = \frac{1}{\frac{\cos^2 \theta}{Ny^2} + \frac{\sin^2 \theta}{Nz^2}}$$

$$Ny' = \frac{Ny Nz}{\sqrt{Nz^2 \cos^2 \theta + Ny^2 \sin^2 \theta}} = \frac{Nz}{\sqrt{\frac{Nz^2}{Ny^2} \cos^2 \theta + (1 - \cos^2 \theta)}} = \frac{Nz}{\sqrt{1 - \nu \cos^2 \theta}}$$

$$\text{HOWEVER, } \nu = \frac{Ny^2 - Nz^2}{Ny^2}$$

WHEN Nz' IS SIMILARLY FOUND

$$\frac{y^2}{Ny^2} + \frac{z^2}{Nz^2} = 1$$

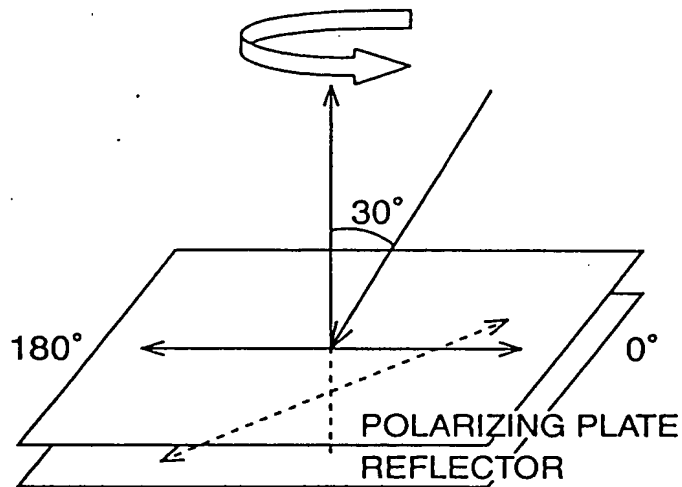
$$\frac{Ny'^2 \sin^2 \theta}{Ny^2} + \frac{Ny'^2 \cos^2 \theta}{Nz^2} = 1$$

$$Ny'^2 = \frac{1}{\frac{\sin^2 \theta}{Ny^2} + \frac{\cos^2 \theta}{Nz^2}}$$

$$Ny' = \frac{Ny Nz}{\sqrt{Nz^2 \sin^2 \theta + Ny^2 \cos^2 \theta}} = \frac{Nz}{\sqrt{\frac{Nz^2}{Ny^2} (1 - \cos^2 \theta) + \cos^2 \theta}} = \frac{Nz}{\sqrt{\frac{Nz^2}{Ny^2} + \nu \cos^2 \theta}}$$

METHOD FOR FINDING REFRACTIVE INDEX ANISOTROPY WHEN LIGHT IS INCIDENT, TILTING θ FROM Z-AXIS, ON LIQUID CRYSTAL AND RETARDATION PLATE

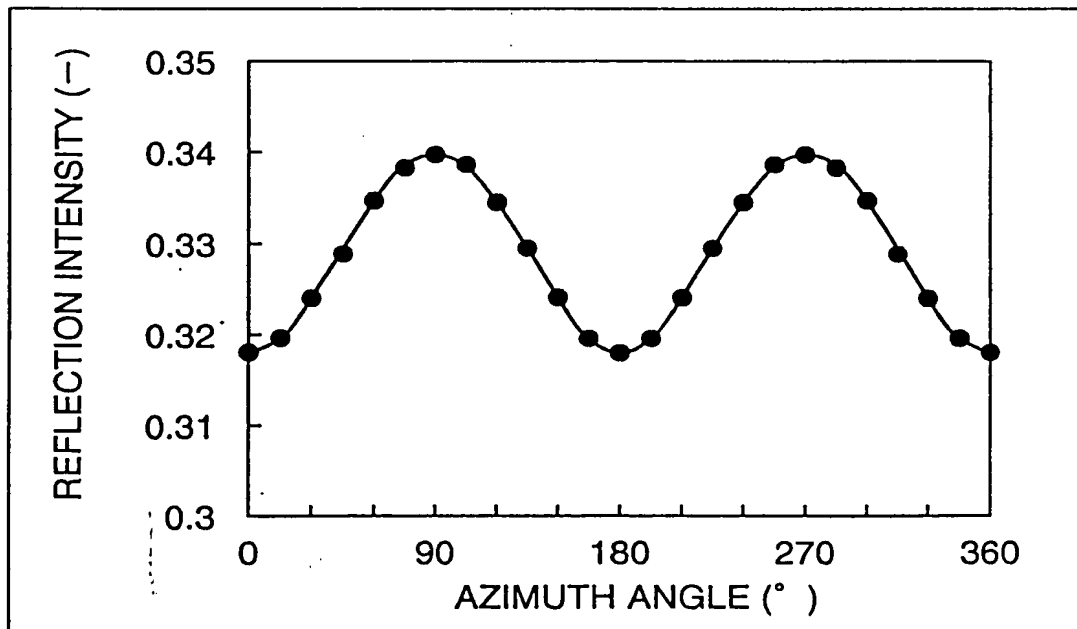
FIG. 16



CONFIGURATION OF SINGLE POLARIZING PLATE AND MEASUREMENT METHOD

THE POLARIZING PLATE WAS ARRANGED SUCH THAT ITS ABSORPTION AXIS WAS IN A 0° AZIMUTH, AND THE REFLECTION INTENSITY WAS MEASURED WITH THE AZIMUTH ANGLE OF A 30°.

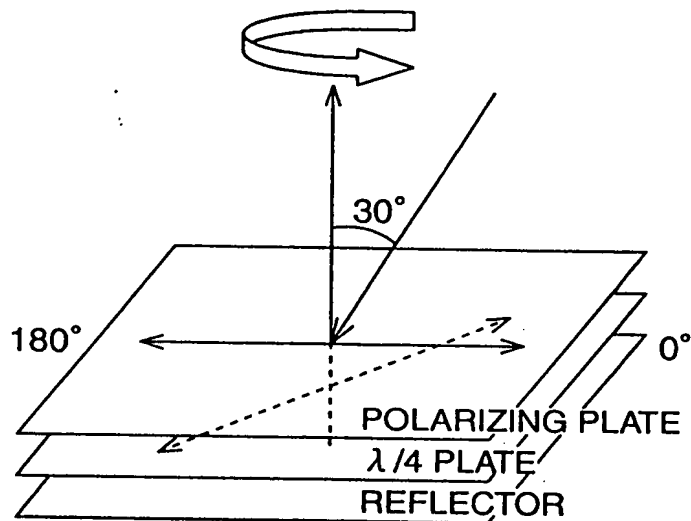
FIG. 17



AZIMUTH ANGLE CHARACTERISTICS OF SINGLE POLARIZING PLATE (30° INCIDENCE)

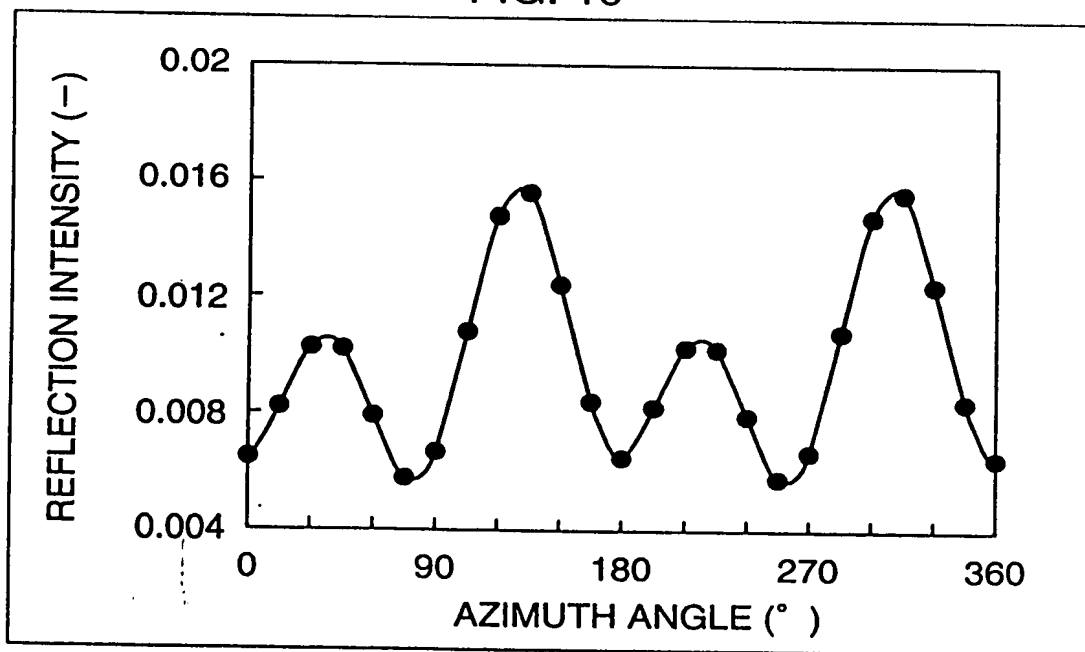
THE REFLECTION INTENSITY IS MINIMUM IN THE ABSORPTION AXIS AZIMUTH (0°, 180°), AND THE REFLECTION IS MAXIMUM IN THE TRANSMISSION AXIS AZIMUTH (90°, 270°).

FIG. 18



CONFIGURATION OF POLARIZING PLATE + $\lambda/4$ AND MEASUREMENT METHOD
 THE $\lambda/4$ PLATE WAS ARRANGED SUCH THAT THE ANGLE FORMED BETWEEN
 ITS SLOW AXIS AND ABSORPTION AXIS WAS 45°, AND THE REFLECTION
 INTENSITY WAS MEASURED WITH THE AZIMUTH ANGLE OF A 30°.

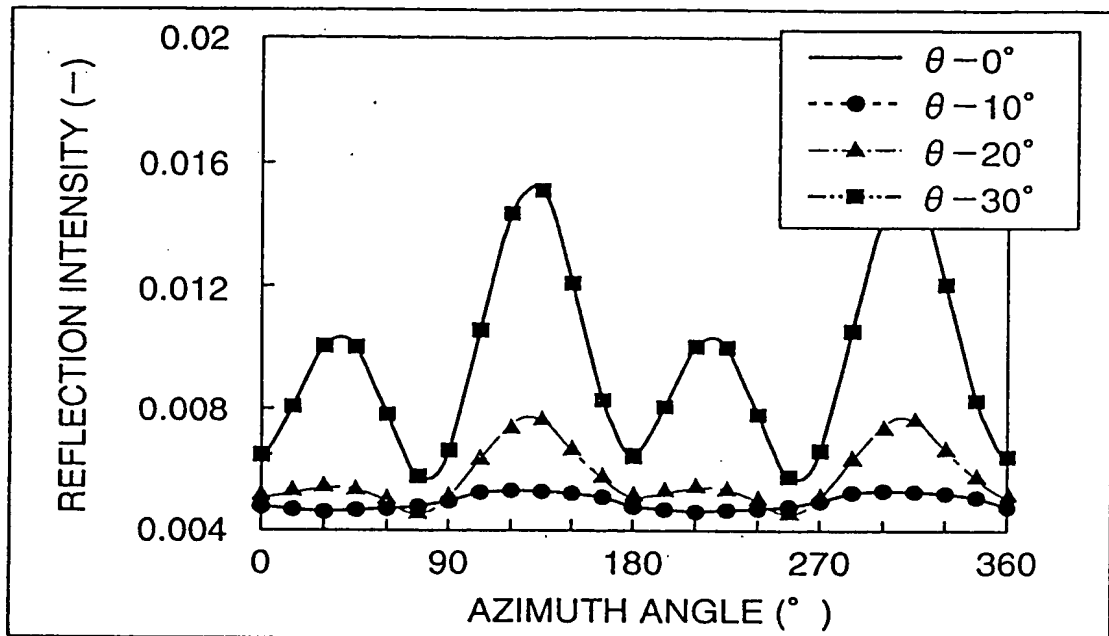
FIG. 19



POLARIZING PLATE + $\lambda/4$ AZIMUTH ANGLE CHARACTERISTICS (1)
 (30° INCIDENCE)

WHEN THE SLOW AXIS OF THE RETARDATION PLATE IS AT 45°,
 THE REFLECTION INTENSITY IS MINIMUM IN THE AZIMUTHS
 DEVIATED BY 45° - 15° FROM THE SLOW AXIS.

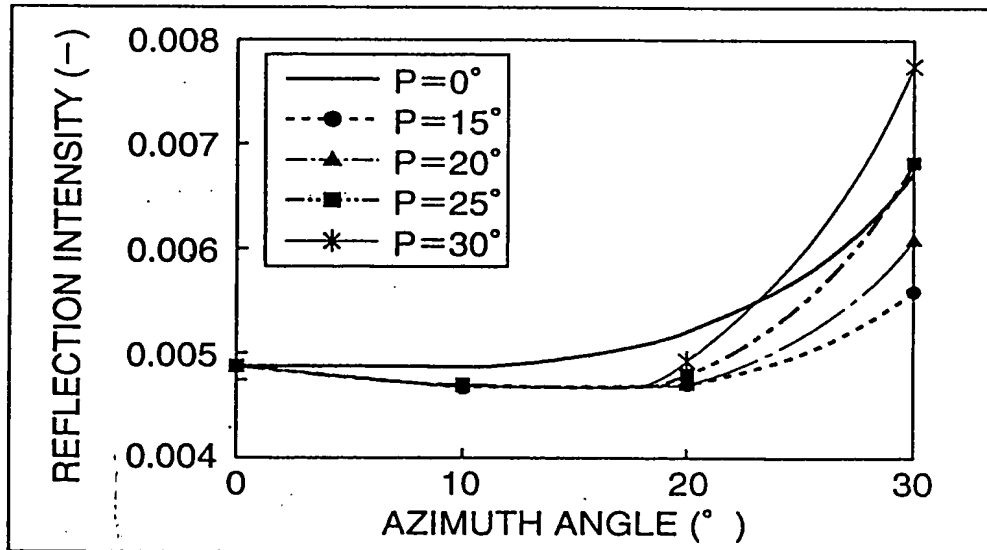
FIG. 20



POLARIZING PLATE + $\lambda/4$ PLATE AZIMUTH ANGLE CHARACTERISTICS (2)
 (0-30° INCIDENT ANGLE)

WITH AN INCREASE IN INCIDENT ANGLE, THE AZIMUTH IN WHICH THE REFLECTION INTENSITY IS MINIMUM INCREASINGLY DEVIATES TO A MINUS AZIMUTH.

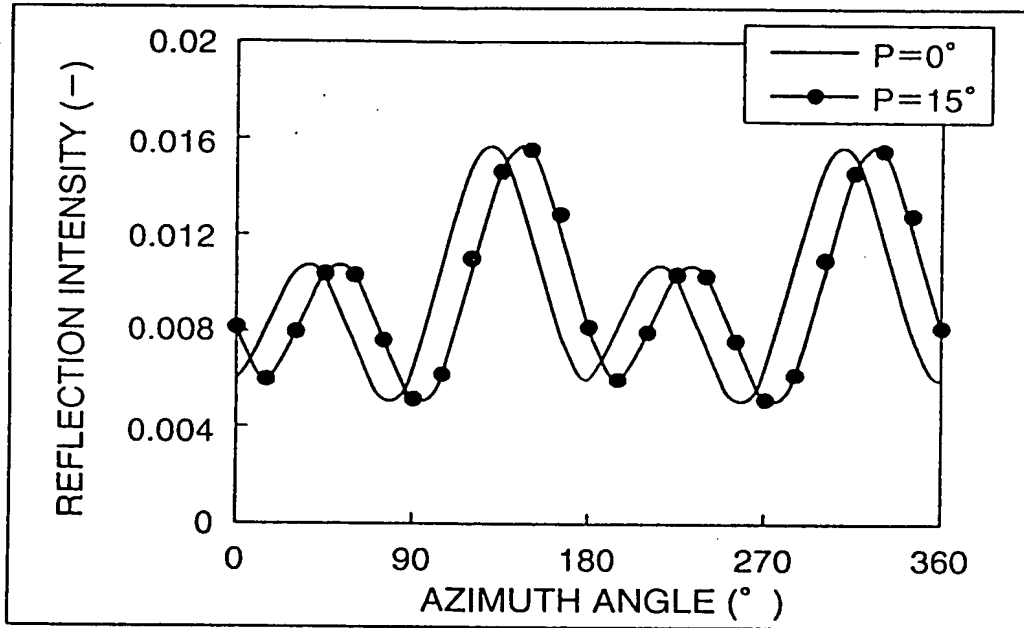
FIG. 21



POLARIZING PLATE + $\lambda/4$ PLATE INCIDENT ANGLE CHARACTERISTICS
 (1) (270° AZIMUTH)

WHEN THE AXIS PLACEMENT IS ROTATED +15° IN AN AZIMUTH OPPOSITE TO THE DEVIATION, THE REFLECTION INTENSITY BECOMES MINIMUM WITHIN THE WHOLE INCIDENT ANGLE RANGE. THE CONTRAST RATIO IS IMPROVED AS COMPARED WITH THAT BEFORE ROTATION WITHIN A RANGE OF 0° TO 25°.

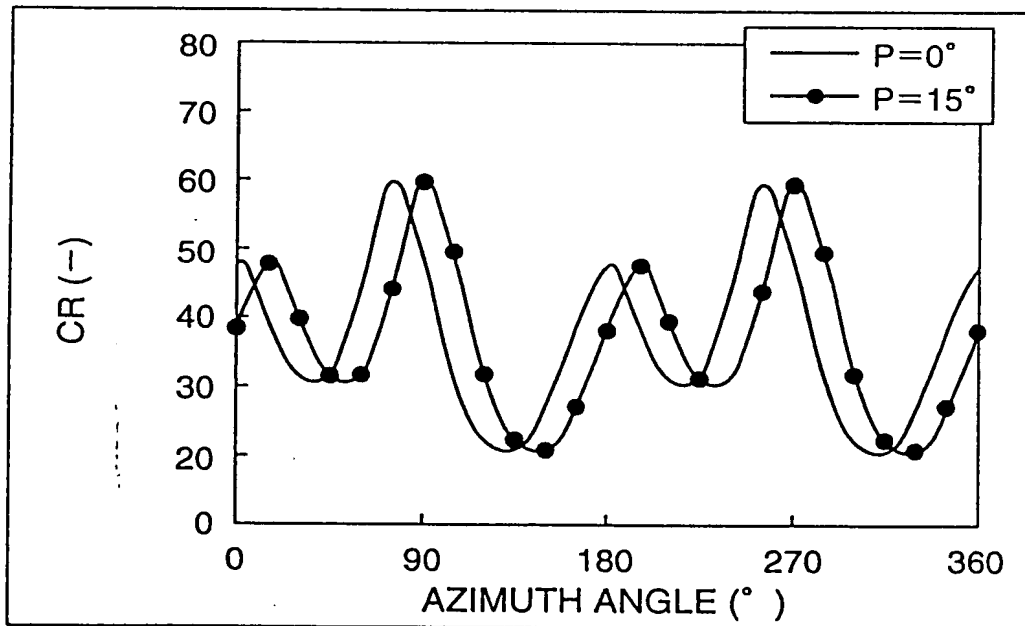
FIG. 22



POLARIZING PLATE + $\lambda/4$ PLATE AZIMUTH ANGLE CHARACTERISTICS (3) (30° INCIDENCE)

WHEN THE AXIS PLACEMENT IS ROTATED +15° IN AN AZIMUTH OPPOSITE TO THE DEVIATION, THE REFLECTION INTENSITY BECOMES MINIMUM IN THE DIRECTIONAL AZIMUTH (90°, 270°).

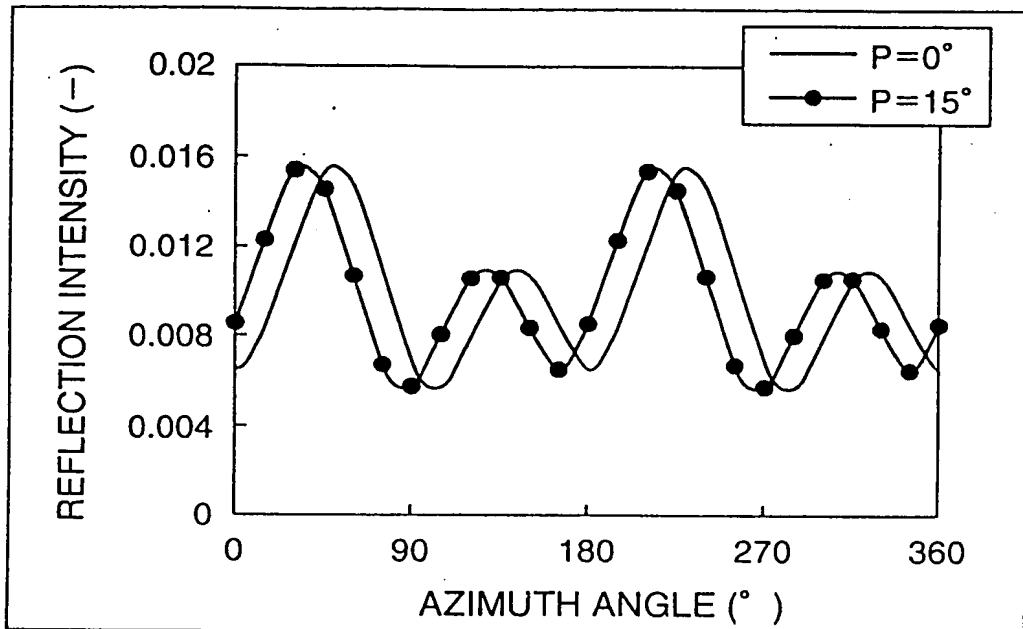
FIG. 23



POLARIZING PLATE + $\lambda/4$ PLATE AZIMUTH ANGLE CHARACTERISTICS (4) (30° INCIDENCE)

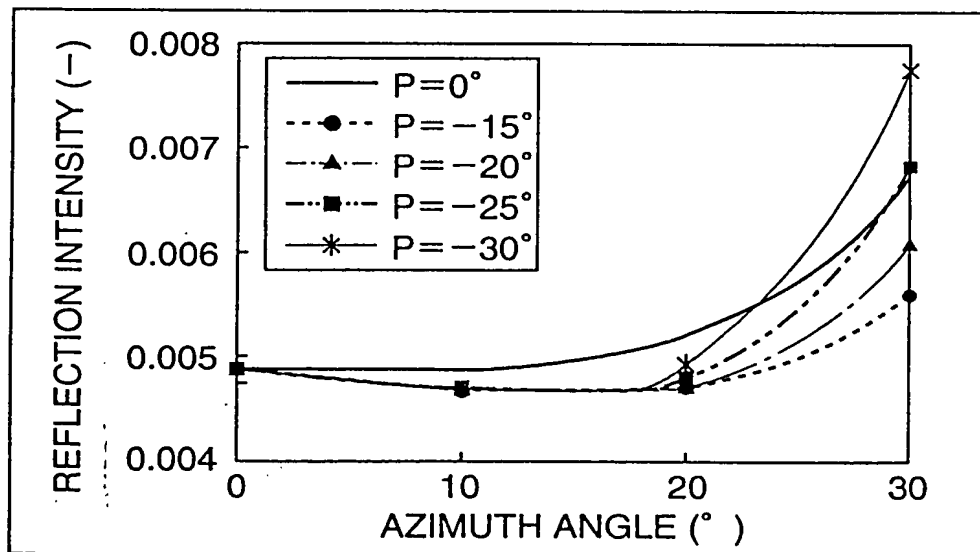
WHEN THE AXIS PLACEMENT IS ROTATED +15° IN AN AZIMUTH OPPOSITE TO THE DEVIATION, CR BECOMES MAXIMUM IN THE DIRECTIONAL AZIMUTH (90°, 270°).

FIG. 24



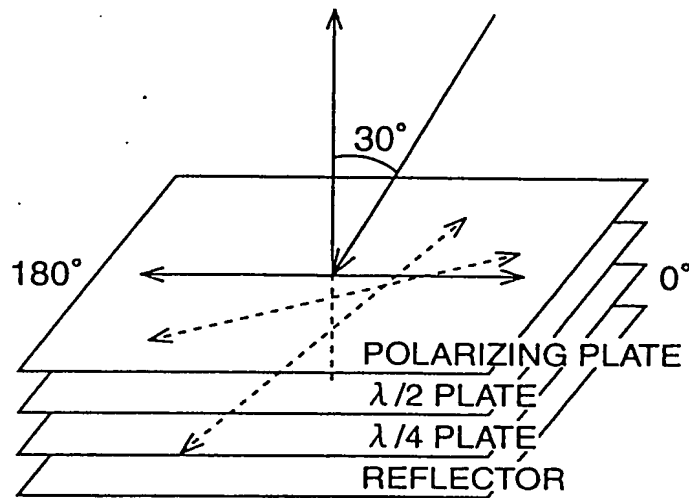
POLARIZING PLATE + $\lambda/4$ PLATE AZIMUTH ANGLE CHARACTERISTICS (5) (30° INCIDENCE)
 WHEN THE SLOW AXIS OF THE RETARDATION PLATE IS AT 135° , THE AZIMUTH IN WHICH THE REFLECTION INTENSITY IS MINIMUM DEVIATES TO A PLUS AZIMUTH. HENCE, THE AXIS PLACEMENT IS ROTATED -15° , WHEREBY THE REFLECTION INTENSITY BECOMES MINIMUM IN THE DIRECTIONAL AZIMUTH.

FIG. 25



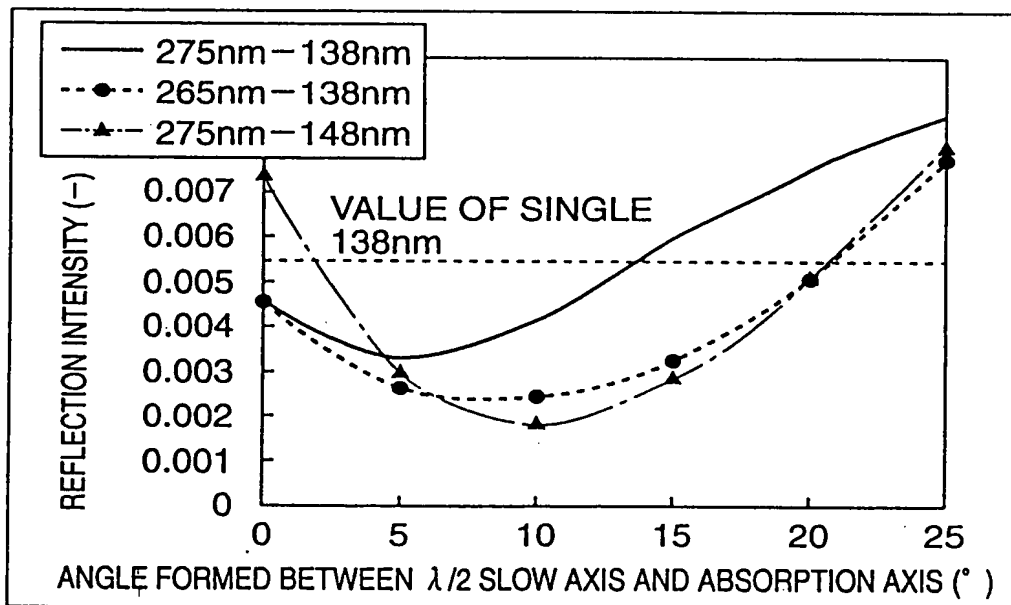
POLARIZING PLATE + $\lambda/4$ PLATE INCIDENT ANGLE CHARACTERISTICS (2) (270° AZIMUTH)
 WHEN THE AXIS PLACEMENT IS ROTATED -15° IN AN AZIMUTH OPPOSITE TO THE DEVIATION, THE REFLECTION INTENSITY BECOMES MINIMUM WITHIN THE WHOLE INCIDENT ANGLE RANGE. THE CONTRAST RATIO IS IMPROVED AS COMPARED WITH THAT BEFORE ROTATION WITHIN A RANGE OF 0° TO -25° .

FIG. 26



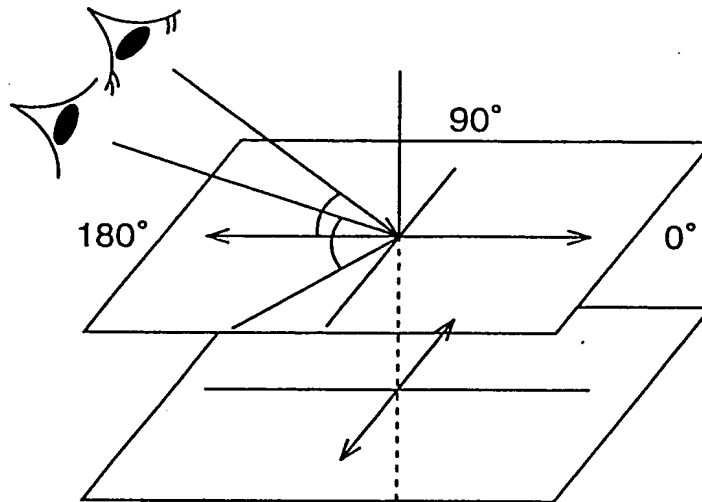
CONFIGURATION OF POLARIZING PLATE + BROADBAND $\lambda/4$ AND MEASUREMENT METHOD
 THE $\lambda/2$ PLATE AND THE POLARIZING PLATE WERE ARRANGED SUCH THAT THE ANGLE FORMED BETWEEN RESPECTIVE SLOW AXIS AND ABSORPTION AXIS WAS 0 TO 25° , AND THE REFLECTION INTENSITY WAS MEASURED WITH RESPECT TO A 30° INCIDENCE.

FIG. 27



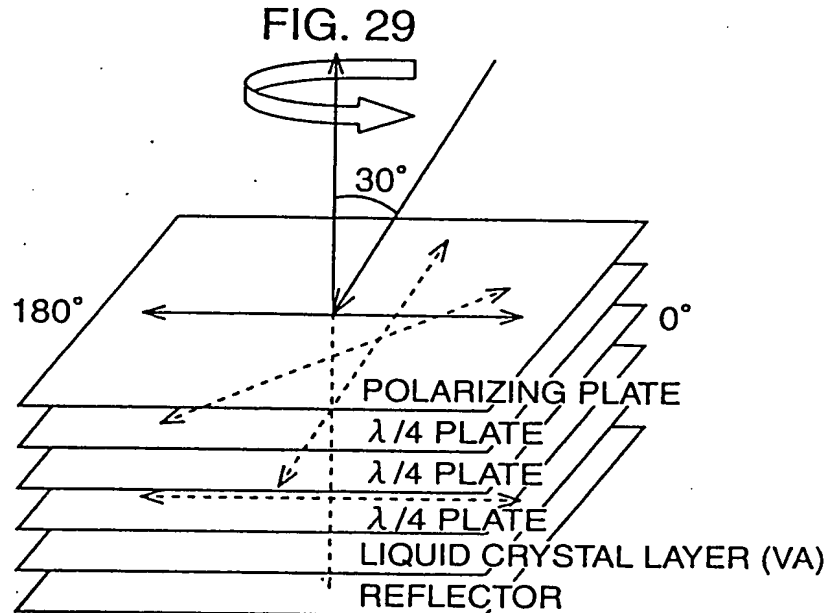
POLARIZING PLATE + BROADBAND $\lambda/4$ PLATE AXIAL CHARACTERISTICS (30° INCIDENCE, 270° AZIMUTH)
 IN A 275nm-138nm COMBINATION, THE REFLECTION INTENSITY BECOMES MINIMUM IN THE DIRECTIONAL AZIMUTH BY SETTING THE ANGLE FORMED BETWEEN THE $\lambda/2$ SLOW AXIS AND THE POLARIZING PLATE ABSORPTION AXIS TO 5° .
 ON THE OTHER HAND IN 265nm-138nm, AND 275nm-148nm COMBINATIONS, THE REFLECTION INTENSITY BECOMES MINIMUM AT THE FORMED ANGLE OF 10° , AND THE OPTIMAL ANGLE DIFFERS DEPENDING ON THE COMBINATION OF RETARDATION PLATES IN USE. IN A RANGE OF AN ANGLE OF 0 TO 20° , THE CONTRAST RATIO IS IMPROVED AS COMPARES TO THAT OF THE SINGLE $\lambda/4$ PLATE.

FIG. 28



AXIS PLACEMENT OF UNIAXIALLY
STRETCHED FILMS
(ORTHOGONAL PLACEMENT)

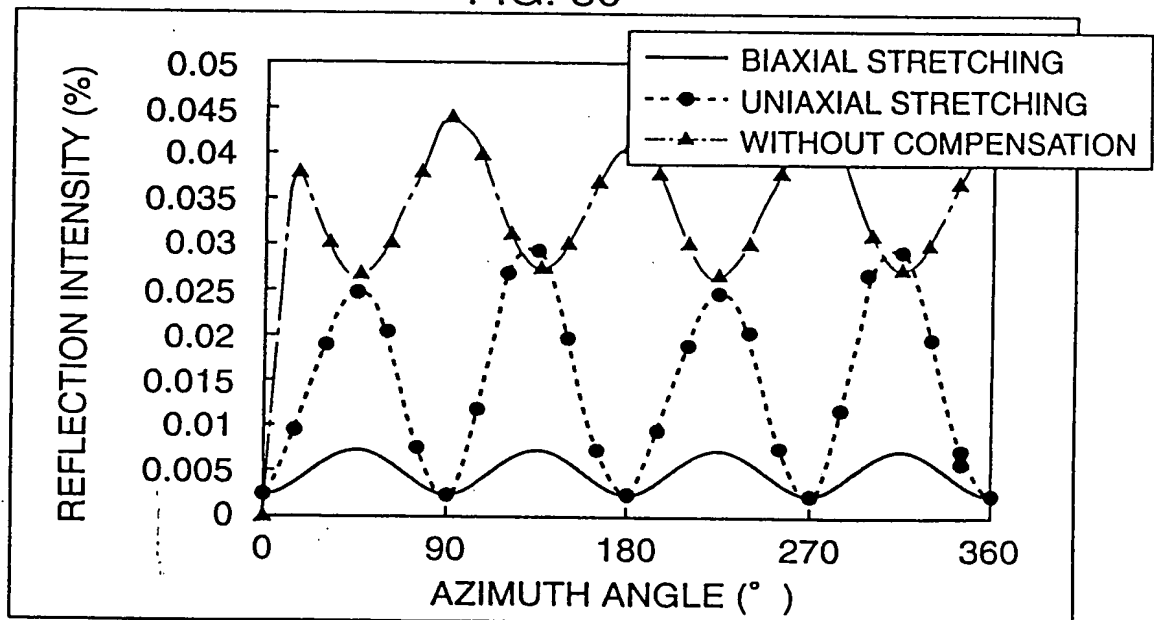
LIGHT LEAKAGE OCCURS IN
AZIMUTHS DIFFERENT FROM THOSE
OF THE SLOW AXES OF
THE UNIAXIALLY FILMS.



CONFIGURATION OF POLARIZING PLATE+ $\lambda/4$ +COMPENSATION PLATE AND MEASUREMENT METHOD

ARRANGEMENT WAS MADE SUCH THAT THE ANGLE FORMED BETWEEN THE DIRECTIONAL AZIMUTH AND THE SLOW AXIS OF THE UNIAXIALLY STRETCHED FILM WAS 0 TO 40°, AND THE REFLECTION INTENSITY WAS MEASURED WITH THE AZIMUTH ANGLE OF A 30° INCIDENCE VARIED.

FIG. 30

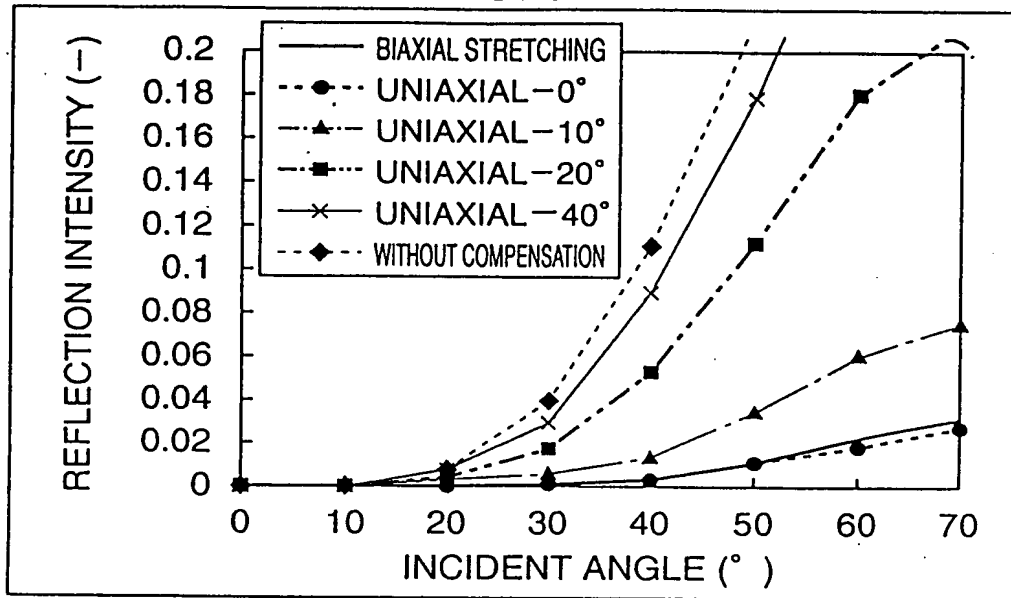


AZIMUTH ANGLE CHARACTERISTICS BY COMPENSATION PLATE (30° INCIDENCE)

UNIAXIAL STRETCHING SHOWS COMPENSATION EFFECTS EQUIVALENT TO THAT BY BIAXIAL STRETCHING IN THE DIRECTIONAL AZIMUTHS.

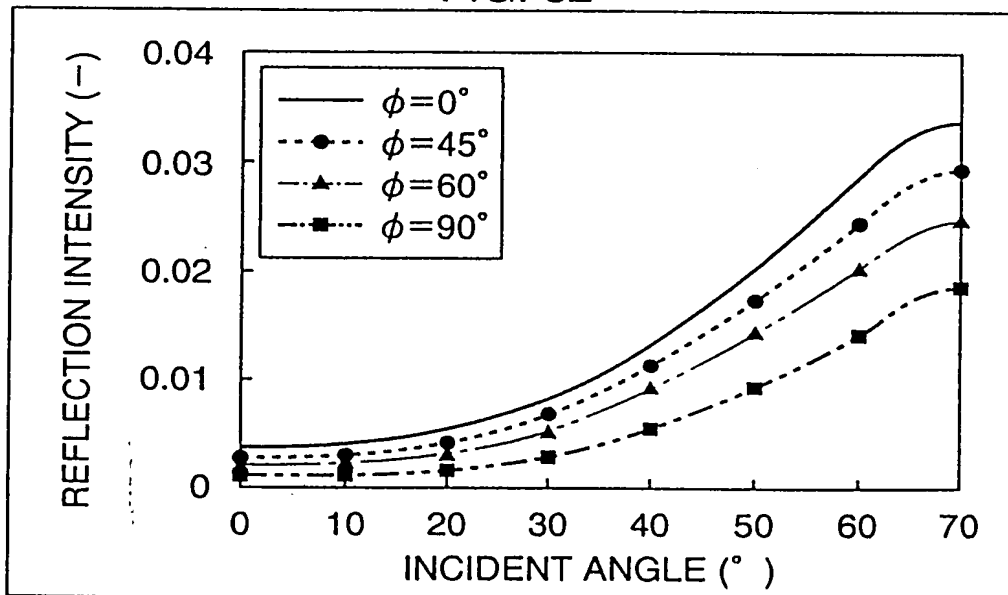
THE REFLECTION INTENSITY IN AZIMUTHS OTHER THAN THE DIRECTIONAL AZIMUTHS DECREASES BY REFLECTING PROJECTIONS AND DEPRESSIONS, SO THAT AZIMUTH DEPENDENCE CAN BE DECREASED.

FIG. 31



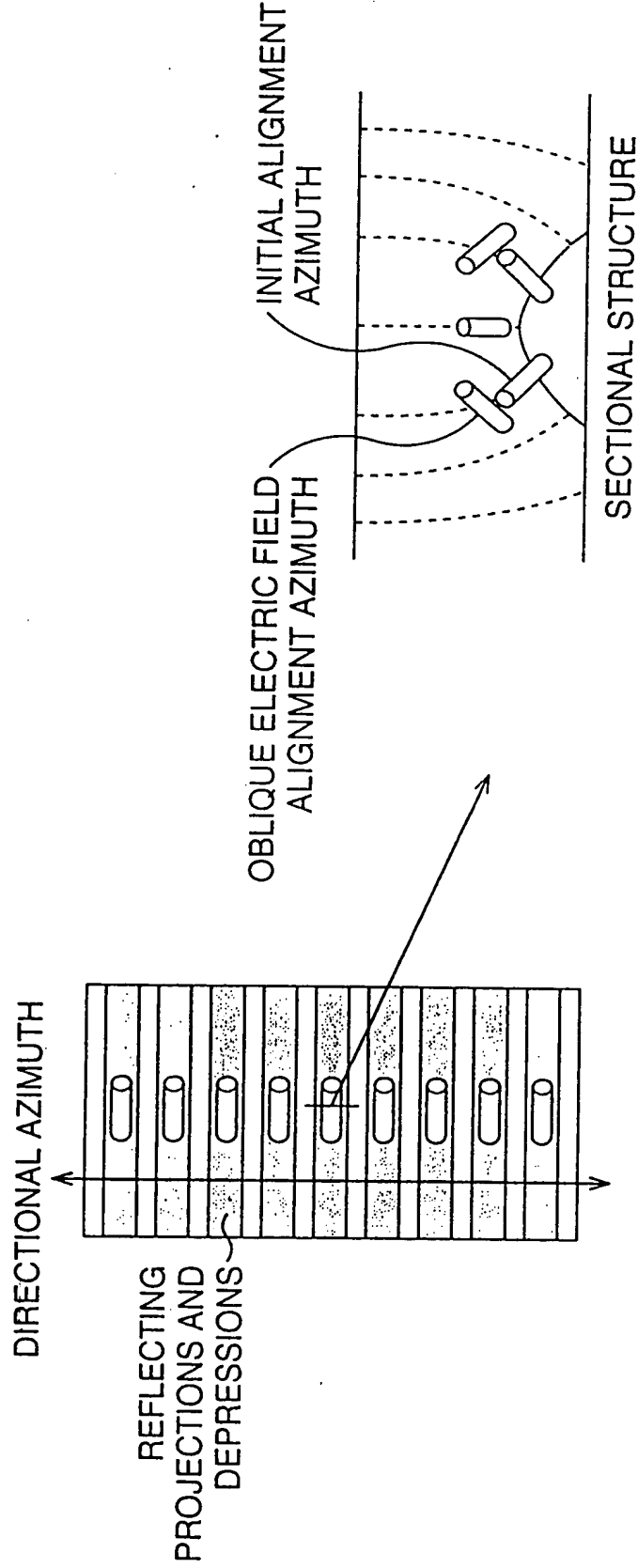
INCIDENT ANGLE CHARACTERISTICS BY COMPENSATION PLATE (270° AZIMUTH)
 WHEN THE ANGLE FORMED BETWEEN THE SLOW AXIS OF THE UNIAXIALLY
 STRETCHED FILM AND THE DIRECTIONAL AZIMUTH IS INCREASED, LIGHT LEAKS
 MORE IN THE APPLICABLE AZIMUTH, BUT WHERE THE ANGLE IS 30° OR LESS,
 THE CONTRAST RATIO CAN BE IMPROVED AS COMPARED TO THE CASE
 WITHOUT COMPENSATION.

FIG. 32



INCIDENT ANGLE CHARACTERISTICS BY ALIGNMENT AZIMUTH (DIRECTIONAL AZIMUTH)
 THE REFLECTION INTENSITY IS MINIMUM AT AN ANGLE FORMED BETWEEN
 THE ALIGNMENT AZIMUTH OF THE LIQUID CRYSTAL AND THE DIRECTIONAL AZIMUTH
 OF 90°, BUT WHERE THE ANGLE IS 45° OR GREATER, SUFFICIENT IMPROVED EFFECTS
 AS COMPARED TO THE CASE OF PARALLEL ALIGNMENT ($\phi=0^\circ$) CAN BE EXPECTED.

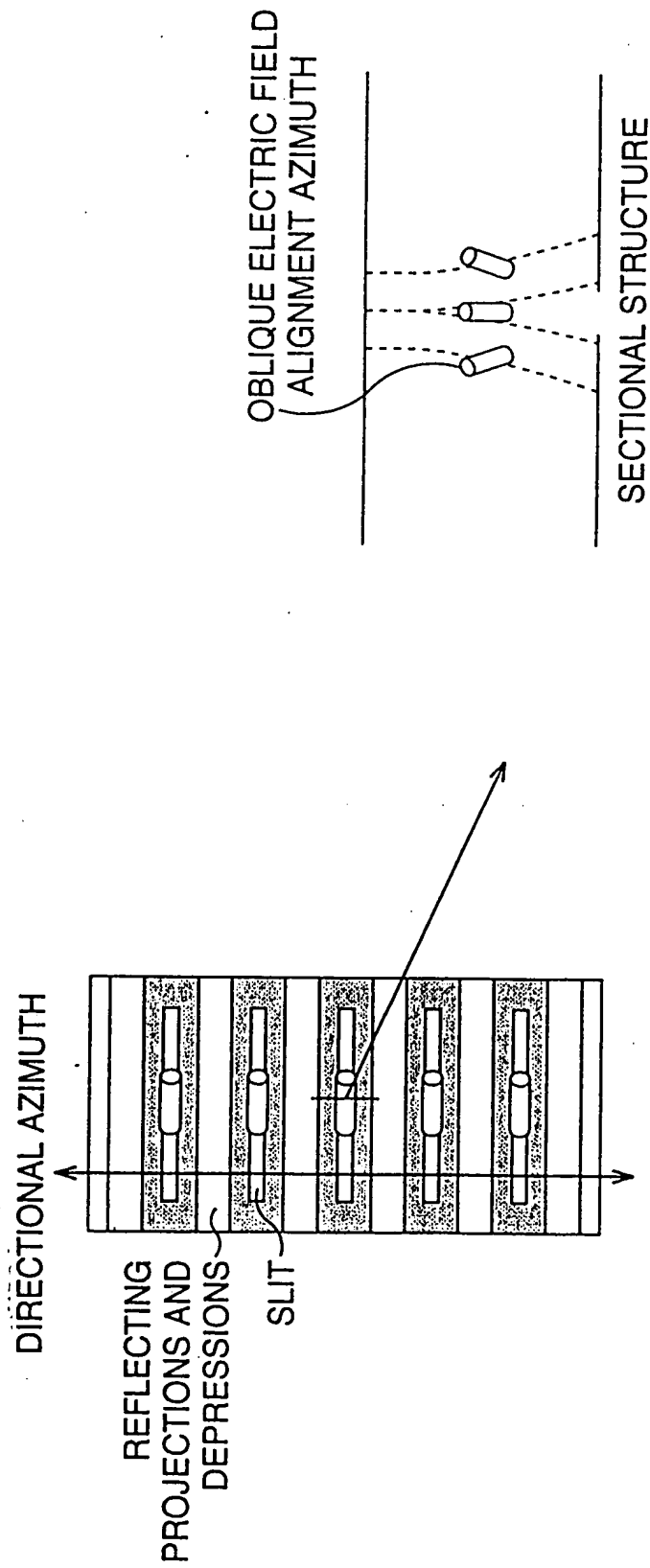
FIG. 33



ALIGNMENT CONTROL USING REFLECTING PROJECTIONS AND DEPRESSIONS

~~THE AZIMUTH IN WHICH THE LIQUID CRYSTAL INITIALLY TILTS AND THE AZIMUTH IN WHICH THE LIQUID CRYSTAL IS TILT-ALIGNED DUE TO AN OBLIQUE ELECTRIC FIELD ARE OPPOSITE, SO THAT THE LIQUID CRYSTAL IS ALIGNED IN AN AZIMUTH DIFFERENT BY ABOUT 90° FROM THE DIRECTIONAL AZIMUTH.~~

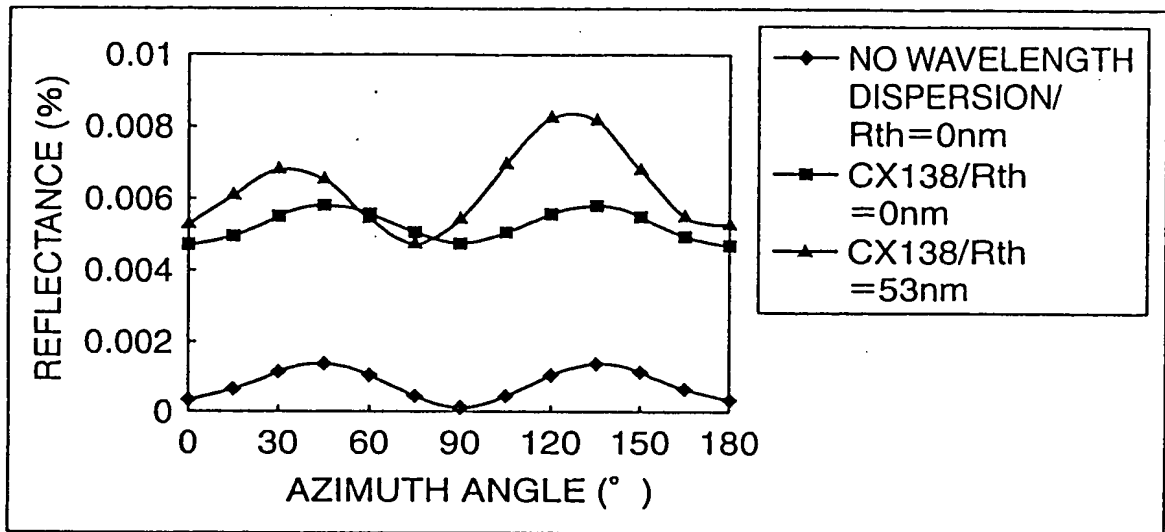
FIG. 34



ALIGNMENT CONTROL USING SLITS

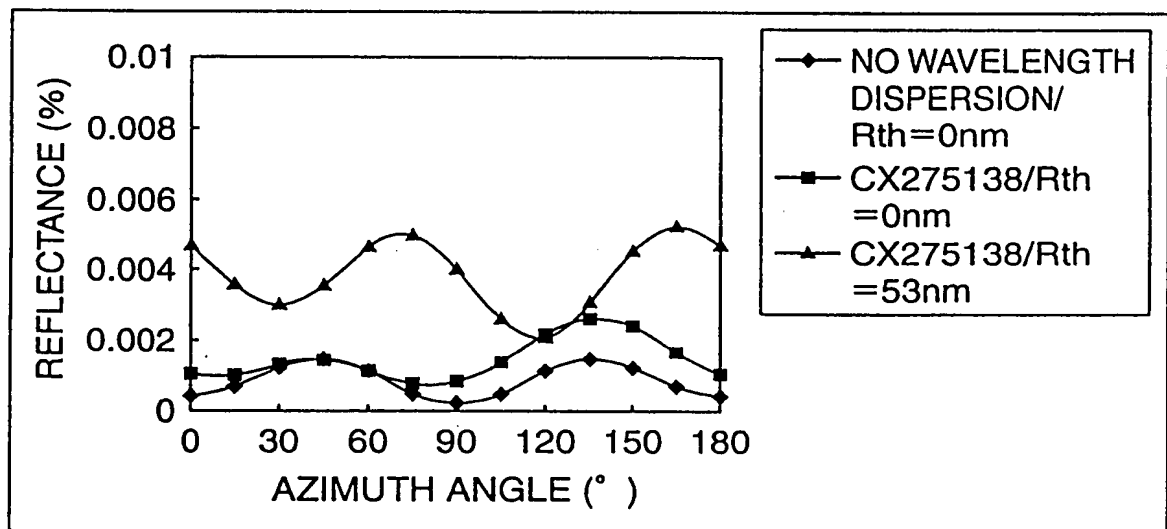
~~WHEN THE SLIT WIDTH IS DECREASED SO THAT THE TILT ALIGNMENT DUE TO AN OBlique ELECTRIC FIELD IS SMALL, THE LIQUID CRYSTAL IS ALIGNED IN AN AZIMUTH DIFFERENT BY ABOUT 90° FROM THE DIRECTIONAL AZIMUTH.~~

FIG. 35A



AZIMUTH DEPENDENCE OF REFLECTANCE OF
 POLARIZING PLATE+ $\lambda/4$ PLATE

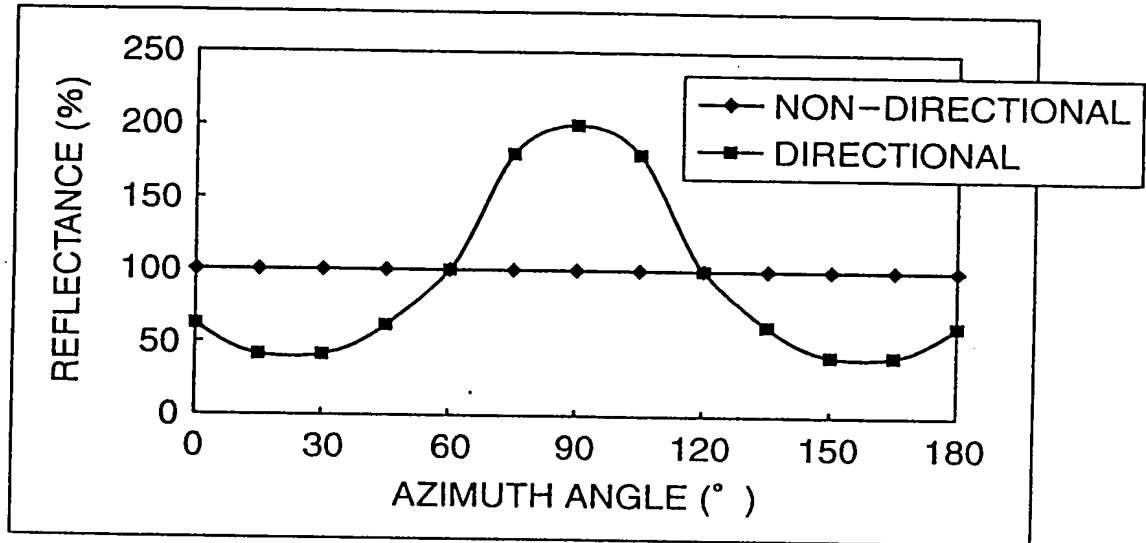
FIG. 35B



AZIMUTH DEPENDENCE OF REFLECTANCE OF
 POLARIZING PLATE+BROADBAND $\lambda/4$ PLATE

THE REFLECTANCE INCREASES DEPENDING ON THE AXIAL AZIMUTH, WAVELENGTH DISPERSION, AND RETARDATION IN THE THICKNESS DIRECTION (R_{th}) OF THE RETARDATION PLATE. FURTHER, THE BROADBAND $\lambda/4$ PLATE HAS LESS WAVELENGTH DISPERSION AND ITS AZIMUTH IN WHICH THE REFLECTANCE IS MINIMUM DEVIATES FROM THE AZIMUTH OF THE POLARIZATION AXIS DEPENDING ON R_{th} . THE DIFFERENCE IN REFLECTANCE BETWEEN THE RETARDATION PLATE HAVING R_{th} AND THE RETARDATION PLATE HAVING NO R_{th} IS THE REFLECTANCE INCREASE DUE TO R_{th} , WHICH IS DIFFERENT DEPENDING ON THE AZIMUTH.

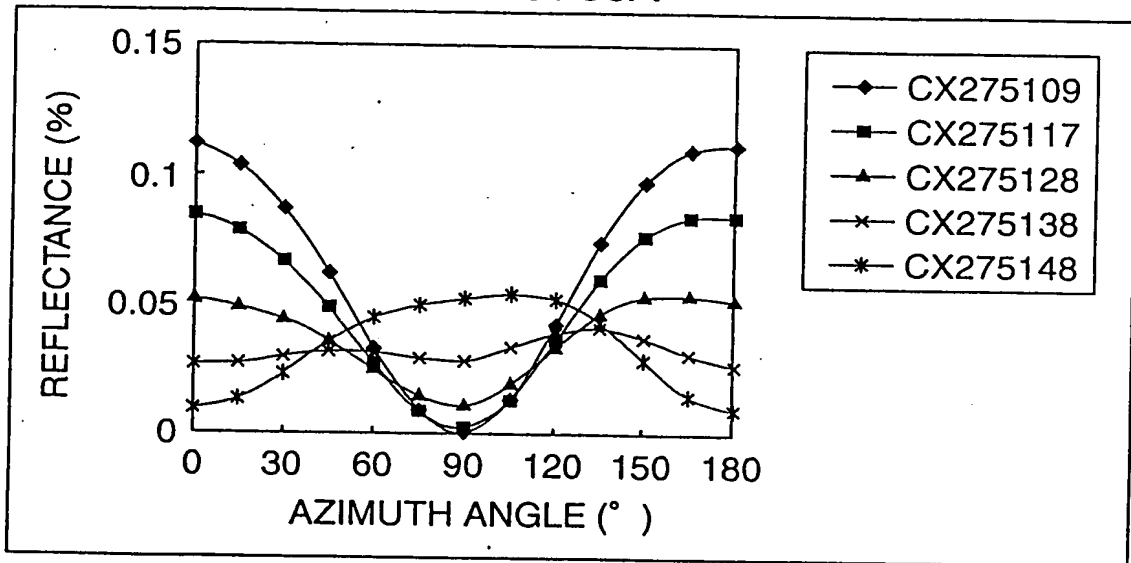
FIG. 37



AZIMUTH DEPENDENCE OF REFLECTANCE OF
REFLECTANCE OF REFLECTOR

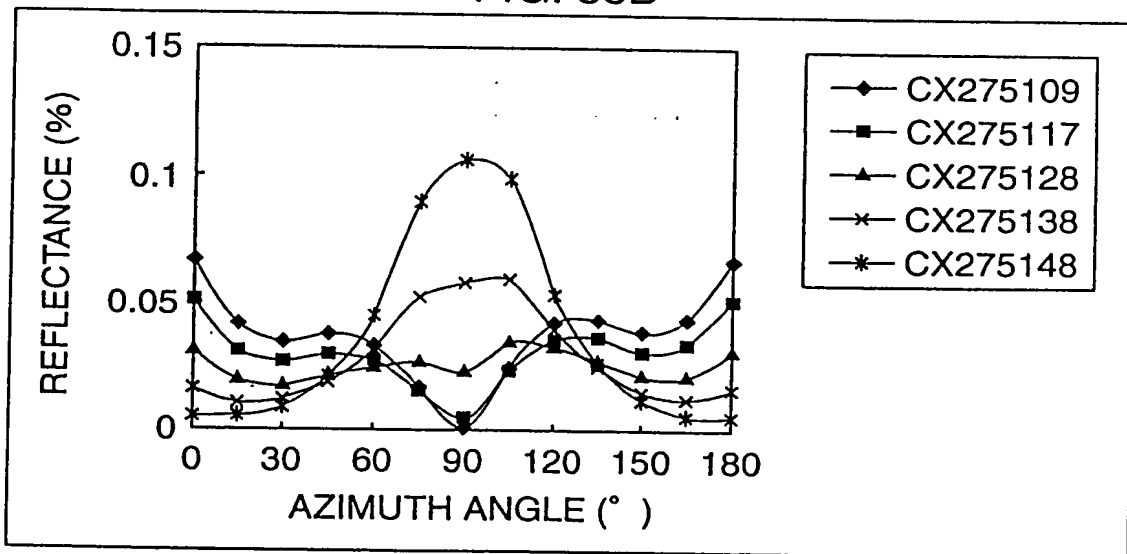
A DIRECTIONAL REFLECTOR SHOWS A REFLECTANCE OF TWICE
THE REFLECTANCE OF A NON-DIRECTIONAL REFLECTOR
IN THE DIRECTIONAL AZIMUTH (90°) AND REFLECTANCE OF
60 PERCENT OF THE REFLECTANCE
IN THE NON-DIRECTIONAL AZIMUTHS.

FIG. 38A



AZIMUTH DEPENDENCE OF REFLECTANCE OF POLARIZING PLATE
 + BROADBAND $\lambda/4$ PLATE+LIQUID CRYSTAL LAYER
 (NON-DIRECTIONAL+ $\lambda/4$ PLATE VARIABLE)

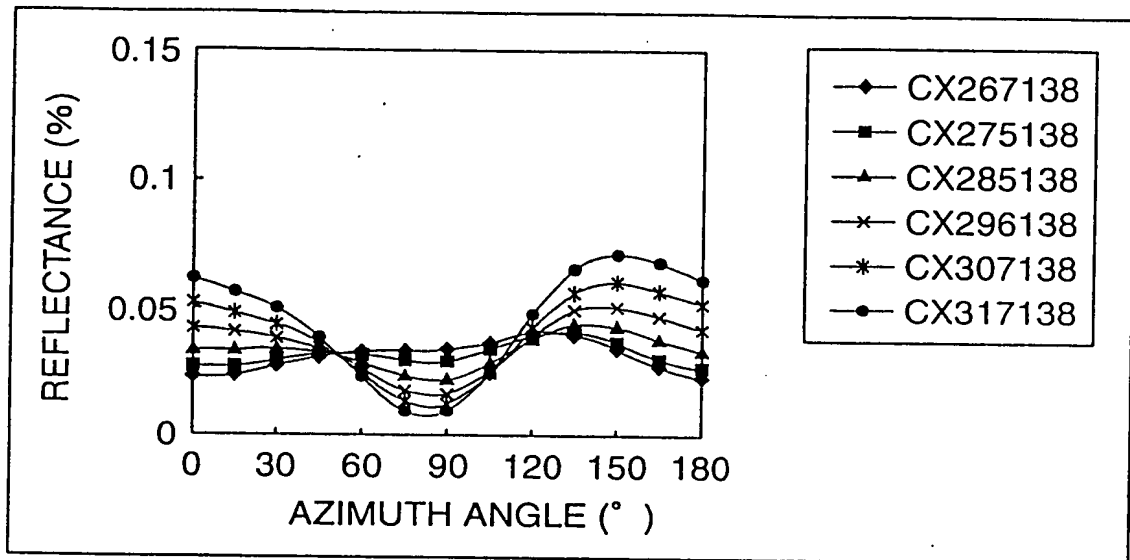
FIG. 38B



AZIMUTH DEPENDENCE OF REFLECTANCE OF POLARIZING PLATE
 + BROADBAND $\lambda/4$ PLATE+LIQUID CRYSTAL LAYER
 (DIRECTIONAL+ $\lambda/4$ PLATE VARIABLE)

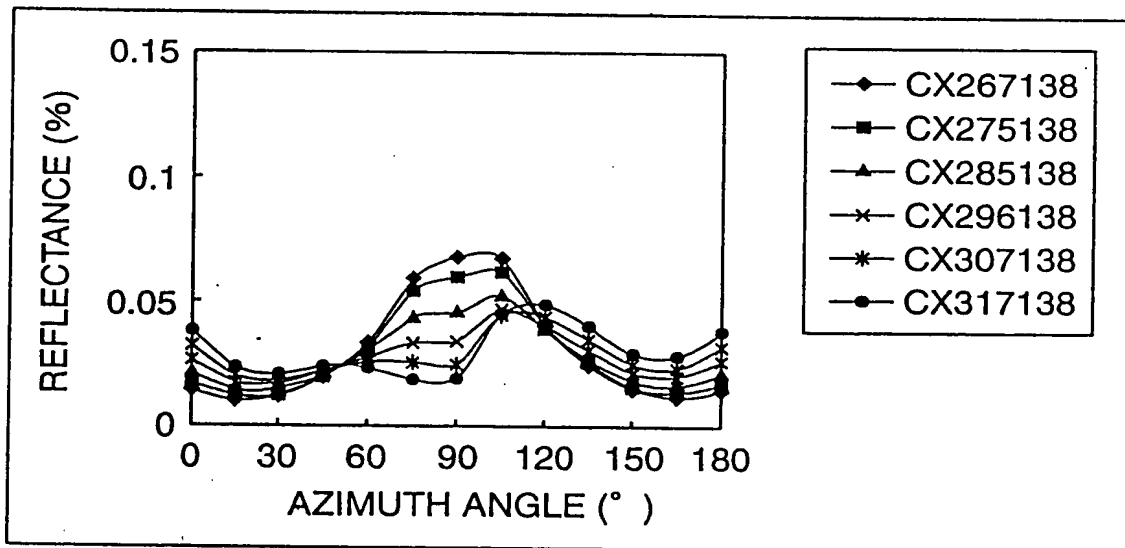
RI INCREASES IN THE DIRECTIONAL AZIMUTH WHEN THE IN-PLANE RETARDATION
 OF THE $\lambda/4$ PLATE IS DECREASED (PREFERABLY, TO ABOUT 110nm TO 120nm),
 SO THAT THE RETARDATION OF THE LIQUID CRYSTAL LAYER IS CORRESPONDINGLY
 COMPENSATED TO DECREASE THE REFLECTANCE. IN CONTRAST TO THE ABOVE,
 RI DECREASES IN THE NON-DIRECTIONAL AZIMUTH TO INCREASE THE REFLECTANCE,
 BUT APPLICATION OF THE DIRECTIONAL REFLECTOR ENABLES THE REFLECTANCE TO BE
 KEPT UNCHANGED FROM THAT BEFORE THE CHANGE OF THE RETARDATION PLATE.

FIG. 39A



AZIMUTH DEPENDENCE OF REFLECTANCE OF POLARIZING PLATE
 + BROADBAND $\lambda/4$ PLATE+LIQUID CRYSTAL LAYER
 (NON-DIRECTIONAL+ $\lambda/2$ PLATE VARIABLE)

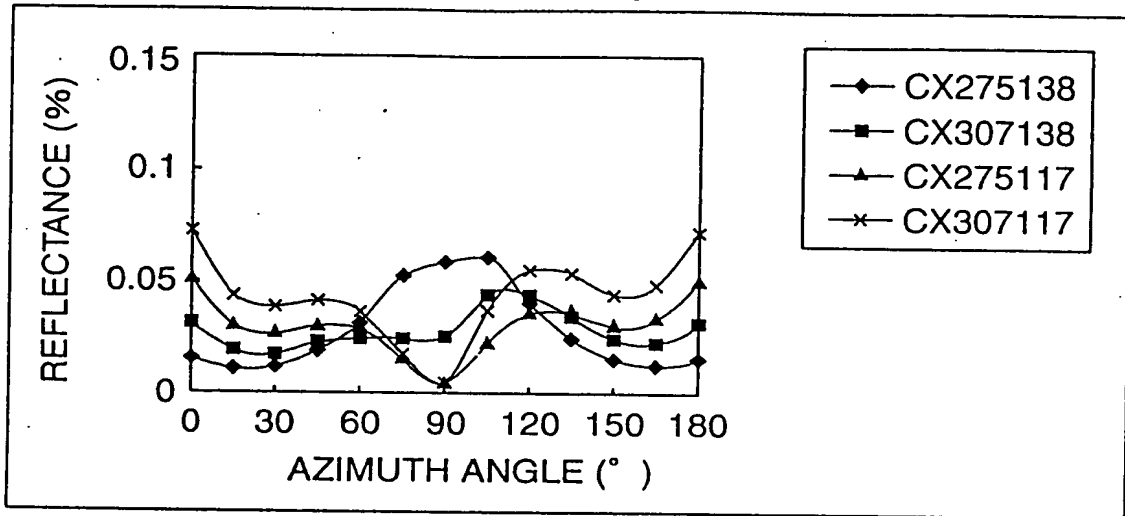
FIG. 39B



AZIMUTH DEPENDENCE OF REFLECTANCE OF POLARIZING PLATE
 + BROADBAND $\lambda/4$ PLATE+LIQUID CRYSTAL LAYER
 (DIRECTIONAL+ $\lambda/2$ PLATE VARIABLE)

~~Rth INCREASES IN THE DIRECTIONAL AZIMUTH WHEN THE IN-PLANE
 RETARDATION OF THE $\lambda/2$ PLATE IS INCREASED (PREFERABLY TO
 ABOUT 300nm TO 320nm), SO THAT THE RETARDATION OF THE LIQUID
 CRYSTAL LAYER IS CORRESPONDINGLY COMPENSATED TO DECREASE
 THE REFLECTANCE.~~

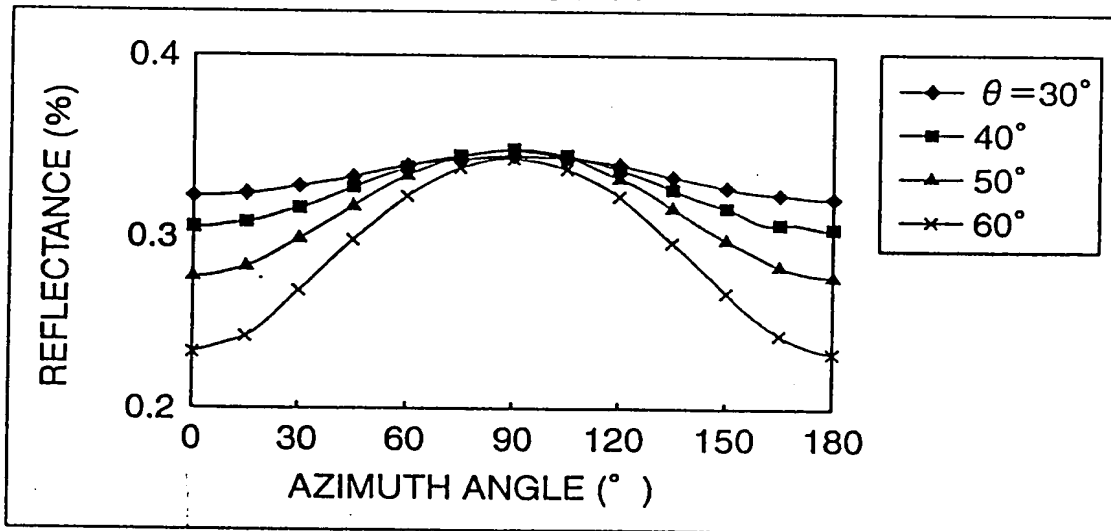
FIG. 40



AZIMUTH DEPENDENCE OF REFLECTANCE OF POLARIZING PLATE
 + BROADBAND $\lambda/4$ PLATE+LIQUID CRYSTAL LAYER
 (DIRECTIONAL, $\lambda/4$ PLATE VARIABLE, $\lambda/2$ PLATE VARIABLE)

~~THE REFLECTANCE IN THE DIRECTIONAL AZIUTH ALSO DECREASES BY CHANGING THE IN-PLANE RETARDATIONS OF BOTH THE $\lambda/4$ PLATE AND THE $\lambda/2$ PLATE. HOWEVER, THE REFLECTANCE INCREASES IN THE NON-DIRECTIONAL AZIMUTH IS MORE MODERATE WHEN THEY ARE INDIVIDUALLY CHANGES.~~

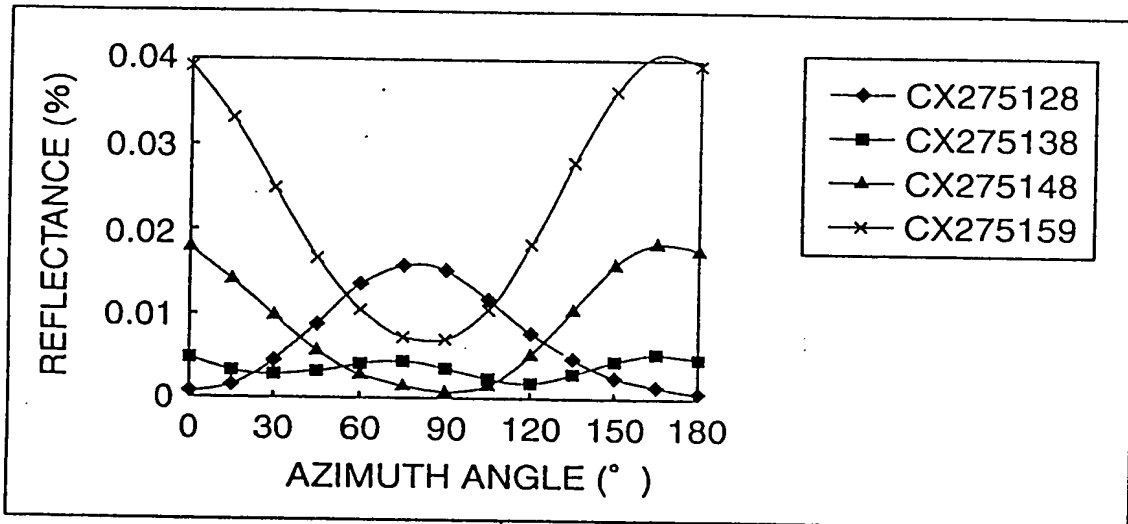
FIG. 41



AZIMUTH DEPENDENCE OF REFLECTANCE OF POLARIZING PLATE
 (θ IS POLAR ANGLE)

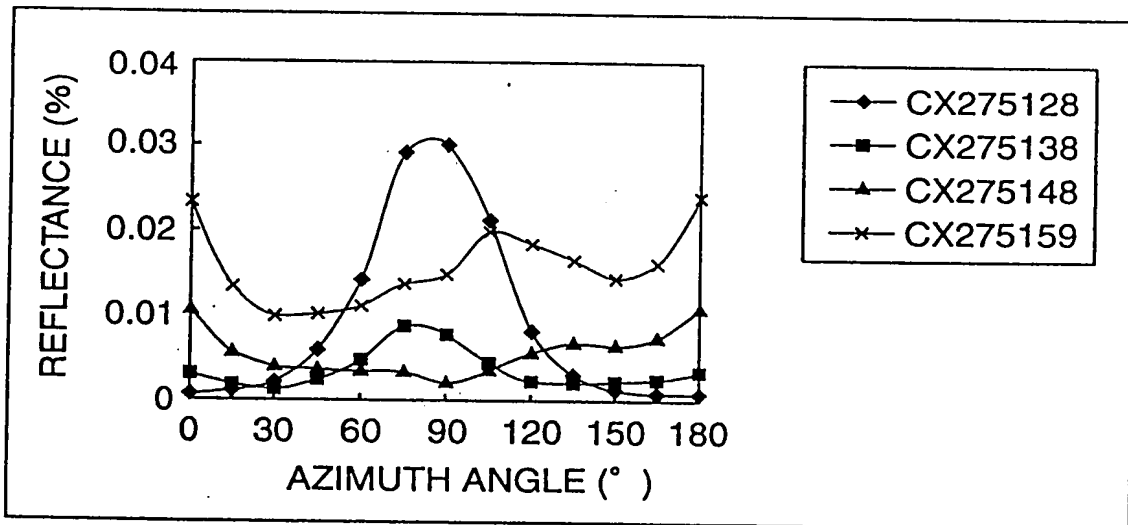
~~THE REFLECTANCE IS DECREASED IN THE AZIMUTH OF THE ABSORPTION AXIS AS ABSORPTION CHARACTERISTICS OF THE POLARIZING PLATE. WHEN THE AXIAL PLACEMENT IS ROTATES 90° , THE MAGNITUDE RELATION BETWEEN THE RESPECTIVE WAVELENGTH PLATES IS REVERSED, BUT THE WHITE REFLECTANCE IS DECREASED IN THE DIRECTIONAL AZIMUTH.~~

FIG. 42A



AZIMUTH DEPENDENCE OF REFLECTANCE OF POLARIZING PLATE
 + BROADBAND $\lambda/4$ PLATE + OPTICAL COMPENSATION PLATE
 + LIQUID CRYSTAL LAYER (NON-DIRECTIONAL + $\lambda/4$ PLATE VARIABLE)

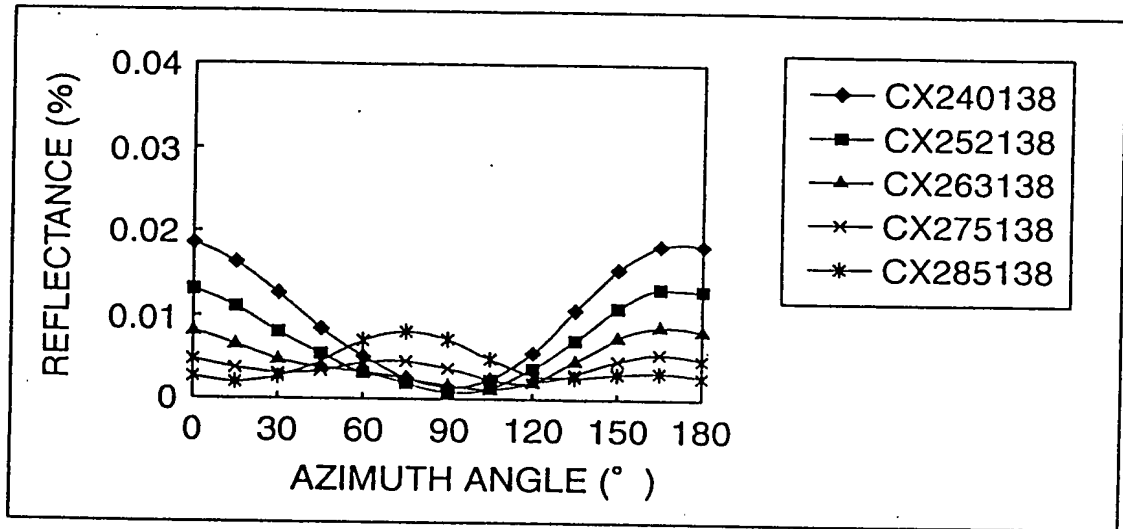
FIG. 42B



AZIMUTH DEPENDENCE OF REFLECTANCE OF POLARIZING PLATE
 + BROADBAND $\lambda/4$ PLATE + OPTICAL COMPENSATION PLATE
 + LIQUID CRYSTAL LAYER (DIRECTIONAL + $\lambda/4$ PLATE VARIABLE)

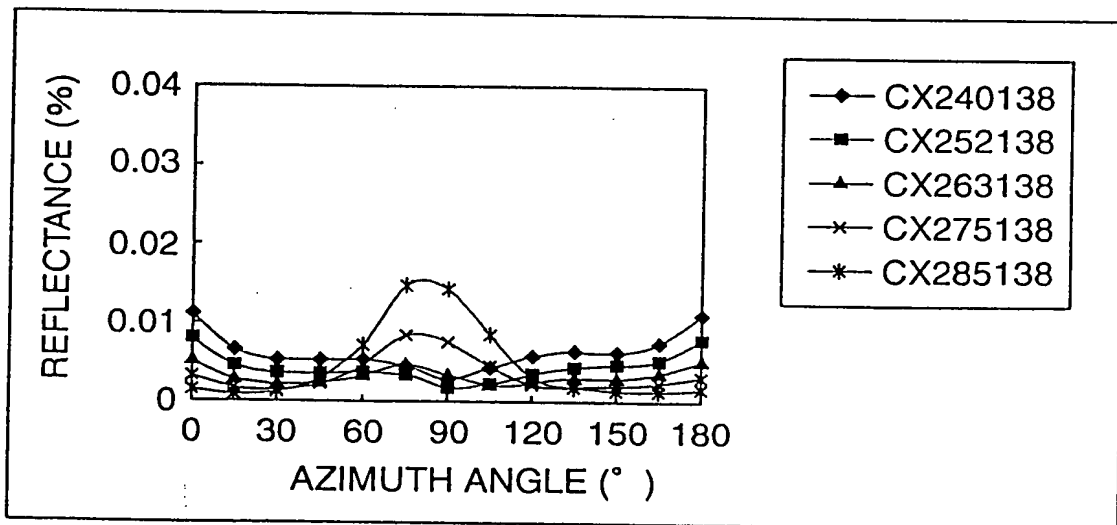
~~WHERE MOST OF THE RETARDATION OF THE LIQUID CRYSTAL
 LAYER IS CANCELED BY THE OPTICAL COMPENSATION PLATE,
 THE REFLECTION CHARACTERISTICS OF THE POLARIZING PLATE
 + THE BROADBAND $\lambda/4$ PLATE ARE REFLECTED. Rth DECREASES IN
 THE RETARDATION OF THE $\lambda/4$ PLATE IS INCREASED (PREFERABLY,
 TO ABOUT 150nm) TO DECREASE THE REFLECTANCE.~~

FIG. 43A



AZIMUTH DEPENDENCE OF REFLECTANCE OF POLARIZING PLATE
 + BROADBAND $\lambda/4$ PLATE + OPTICAL COMPENSATION PLATE
 + LIQUID CRYSTAL LAYER (NON-DIRECTIONAL + $\lambda/2$ PLATE VARIABLE)

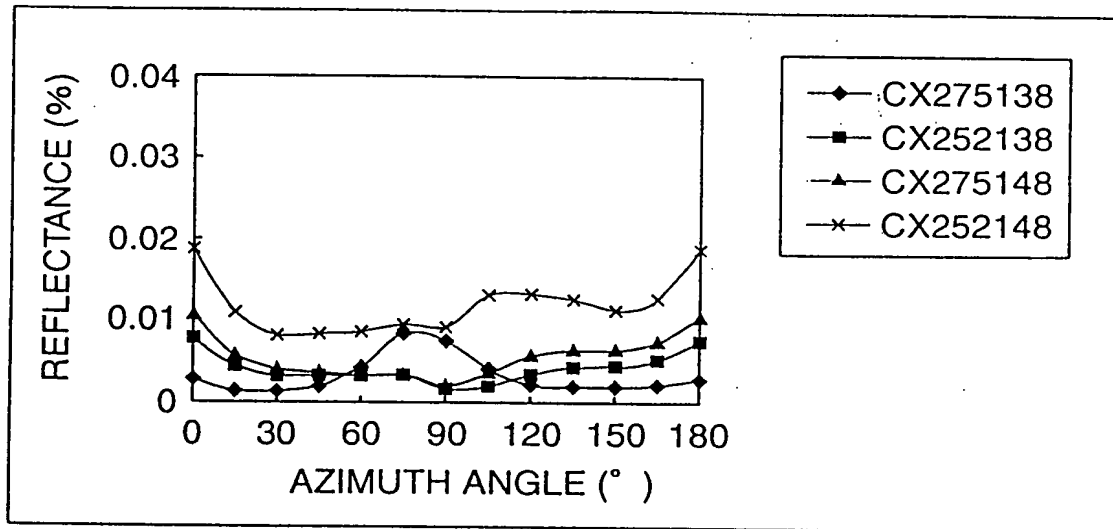
FIG. 43B



AZIMUTH DEPENDENCE OF REFLECTANCE OF POLARIZING PLATE
 + BROADBAND $\lambda/4$ PLATE + OPTICAL COMPENSATION PLATE
 + LIQUID CRYSTAL LAYER (DIRECTIONAL + $\lambda/2$ PLATE VARIABLE)

~~R_{th} DECREASES IN THE DIRECTIONAL AZIMUTH WHEN
 THE RETARDATION OF THE $\lambda/2$ PLATE IS DECREASES
 (PREFERABLY TO ABOUT 240 TO 260nm),
 SO THAT THE REFLECTANCE IS DECREASED.~~

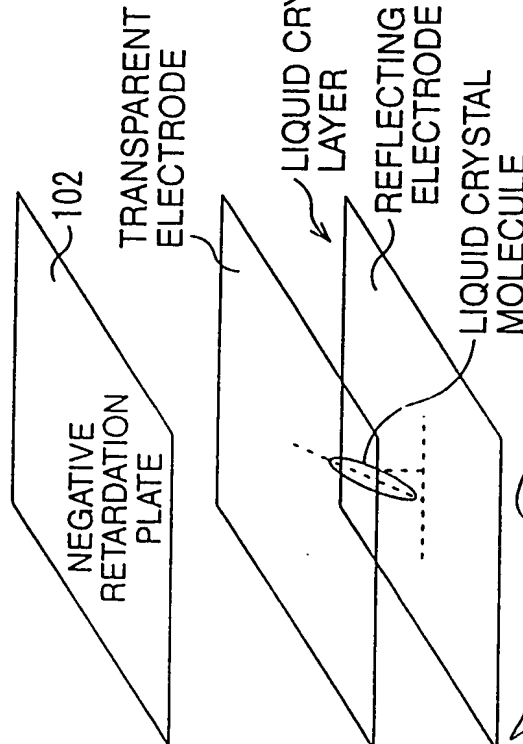
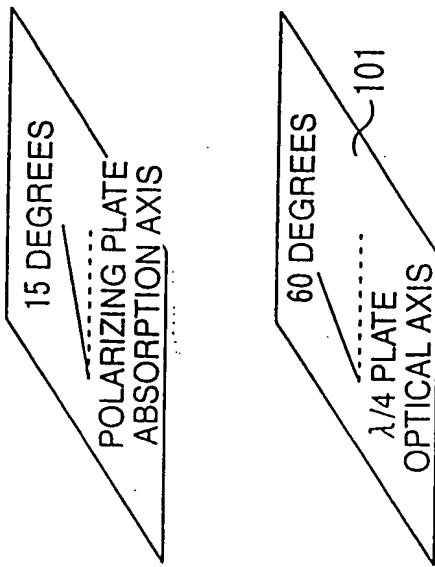
FIG. 44



AZIMUTH DEPENDENCE OF REFLECTANCE OF POLARIZING PLATE
 + BROADBAND $\lambda/4$ PLATE + OPTICAL COMPENSATION PLATE
 + LIQUID CRYSTAL LAYER
 (DIRECTIONAL, + $\lambda/2$ PLATE VARIABLE, $\lambda/4$ PLATE VARIABLE)

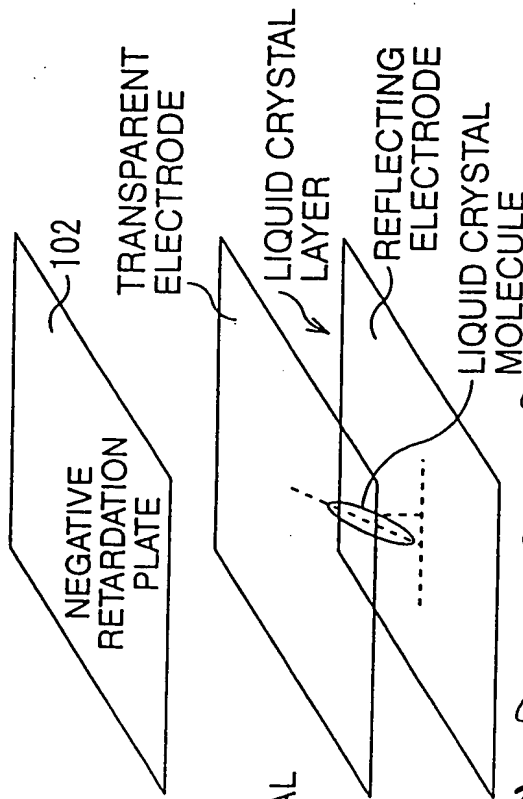
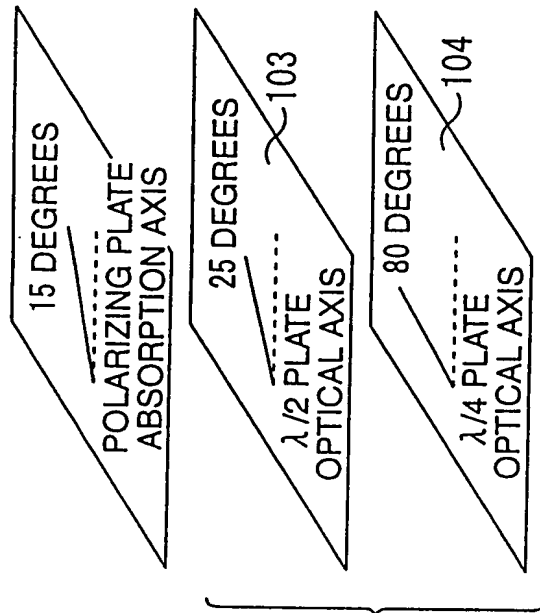
~~THE REFLECTANCE INCREASES WHEN
 THE IN-PLANE RETARDATIONS OF
 BOTH THE $\lambda/2$ PLATE AND THE $\lambda/4$ PLATE ARE CHANGED.~~

FIG. 45A PRIOR ART



~~VERTICALLY ALIGNED LIQUID CRYSTAL MOLECULE FILMS IN A 0-DEGREE AZIMUTH WHERE VOLTAGE IS APPLIED~~

FIG. 45B PRIOR ART



~~VERTICALLY ALIGNED LIQUID CRYSTAL MOLECULE FILMS IN A 0-DEGREE AZIMUTH WHERE VOLTAGE IS APPLIED~~